

Tentative Designs for X-Band and W-Band Klystrons with Corkscrew-Modulated Hollow Electron Beam

Heino Henke | Theoretische Elektrotechnik | Technische Universität Berlin |
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Introduction

X-Band Klystron Design

W-Band Klystron Design

Electron Gun for Generating a Hollow Beam

Conclusions

Introduction

Why a klystron ?

- **high RF power**
- **high reliability**
- **various applications in the industry**

Why a klystron with hollow beam ?

- **higher beam power**
- **easily beam focussing strategy**
- **larger klystron structure**



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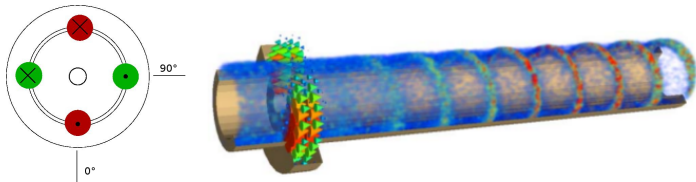
¹ A klystron as used in the storage ring at the Australian Synchrotron, Clayton, Victoria.
<https://commons.wikimedia.org/wiki/File:Aust.-Synchrotron,-Klystron-for-Storage-Ring,-14.06.2007.jpg>

Introduction

- **X-Band Klystron with Hollow Beam for Power Amplification**
- **W-Band Klystron with Hollow Beam for Power Amplification and Frequency Tripling**

A modulated hollow beam has three components:

- hollow beam
- resonant cavity operating in rotating TM_{m10} -mode
- hollow beam modulated by rotating mode in propagation direction



X-Band Klystron Design

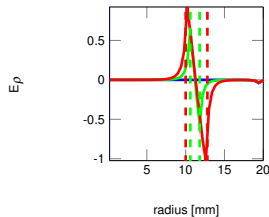
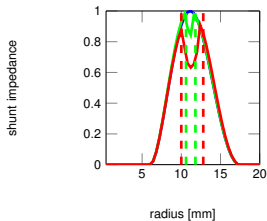
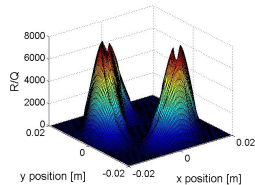
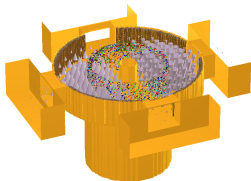
- TM₁₁₀-mode Klystron

important parameters

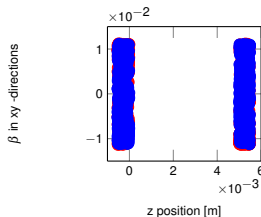
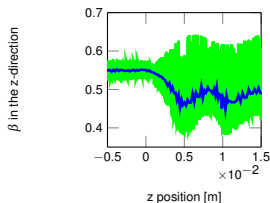
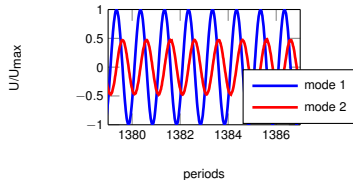
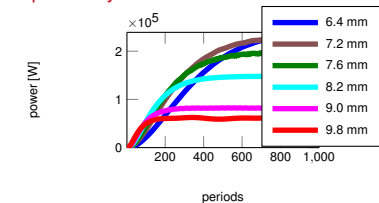
- **operating frequency:** 10GHz
- **mode in the cavities:** TM₁₁₀-mode
- **beam velocity:** $0.55 \cdot c_0$
- **beam voltage:** 100kV
- **beam power:** 1 MW

- TM_{110} -mode Klystron output cavity

- one-gap cavity



- TM₁₁₀-mode Klystron output cavity

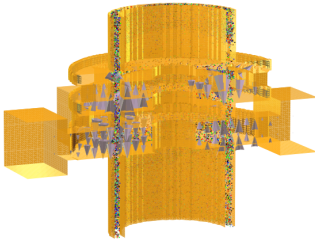


Velocity of electrons in the output cavity with an aperture width of 7.6 mm; left: β of electrons in z-direction in solid green line and average β in solid blue line; right: β of electrons in x-direction (blue dots) and in y-direction (red dots) before and after the travelling in output cavity

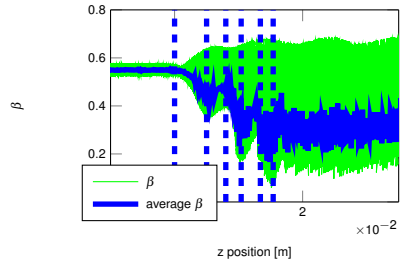
- TM_{110} -mode Klystron

output cavity

○ three-gap cavity



Three-gap structure excited in π mode, gap lengths are tapered

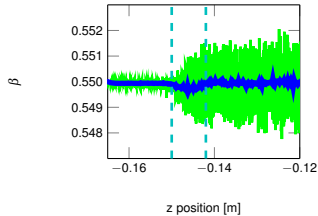
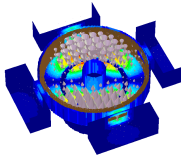


cavity	\bar{P}_{out}	β	$\bar{P}_{out}/\bar{P}_{int}$
one-gap	210 kW	0.35	5.3
two-gaps	310 kW	0.20	4.9
three-gap	460 kW	0.13	5.0

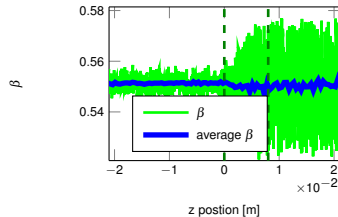
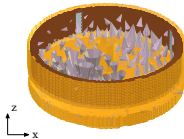
- TM₁₁₀-mode Klystron

input and idler cavities

○ input cavity



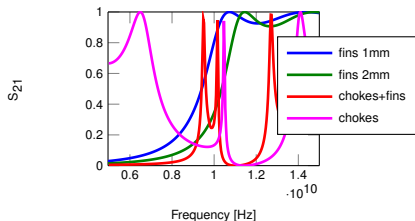
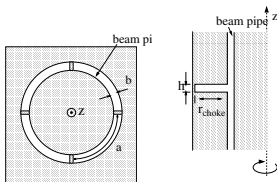
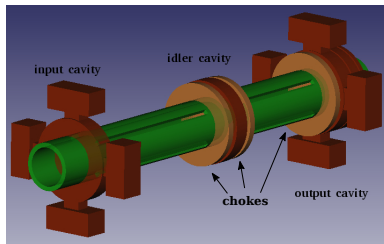
○ idler cavity



- TM_{110} -mode Klystron

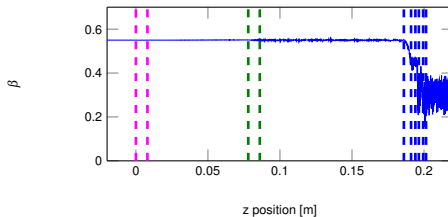
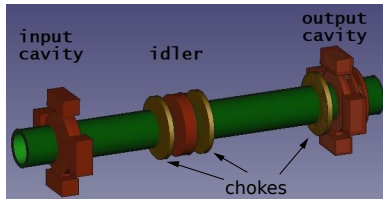
isolation strategy

- **choke**
- bandstop filter
- **fins**
- high-pass filter



Top view of four fins which connect inner and outer conductors (left); side view of a radial transmission line as choke (right)

- TM₁₁₀-mode Klystron
whole klystron

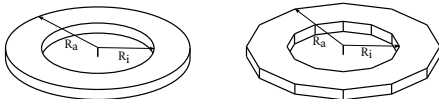


$$\bar{P}_{out} = 500 \text{ kW}$$

Normalized velocity β of electrons in TM₁₁₀ X-band klystron with chokes

X-Band Klystron Design

- TM_{310} -Mode Klystron



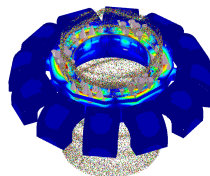
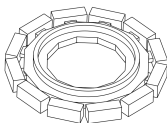
important parameters

- **operating frequency:** 10 GHz
- **mode in the cavities:** TM_{310} -mode
- **beam velocity:** $0.55 \cdot c_0$
- **beam voltage:** 100 kV
- **beam power:** 5 MW

- TM₃₁₀-mode Klystron

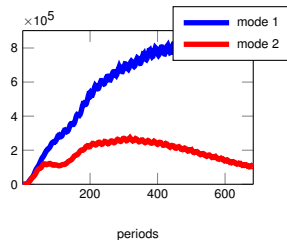
output cavity

- output cavity with 12 couplers



cavity	\bar{P}_{out}	η	$\bar{P}_{out}/\bar{P}_{int}$
one gap	1.20 MW	24%	9
two gaps	1.80 MW	36%	9

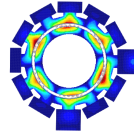
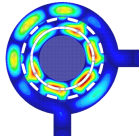
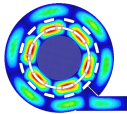
power [W]



- TM₃₁₀-mode Klystron

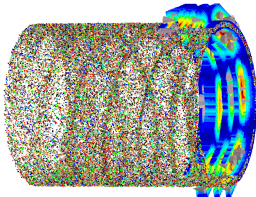
output cavity

- output cavity with fewer than 12 couplers



only the third configuration works

- output cavity without couplers

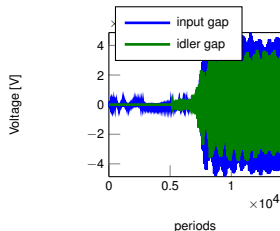
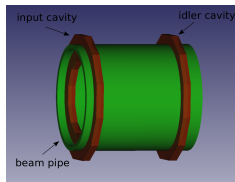


cavity	average β	\bar{P}_{out}
three-gap	0.40	2.29 MW
four-gap	0.38	2.51 MW

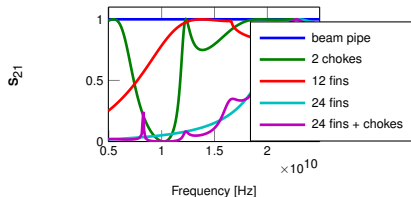
- TM₃₁₀-mode Klystron

input and idler cavities

Coaxial beam pipe connects the input cavity and the idler cavity

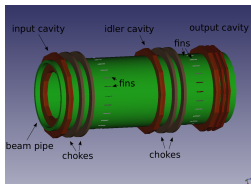


S_{21} of beam pipe with different filters

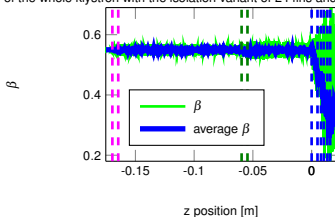


- TM₃₁₀-mode Klystron

whole klystron



Configuration of the whole klystron with the isolation variant of 24 fins and 2 chokes



Normalized velocity β of electrons while the beam is moving through the klystron operating in the TM₃₁₀-mode

$$U_{new} = \frac{m_e c^2}{e} \sqrt{\frac{1}{1 - \left(\frac{\beta_{new} \cdot c_0}{c_0}\right)^2} - 1} \quad (1)$$

$$\bar{P}_{out} = (U - U_{new}) I \cdot \frac{\beta_K}{1 + \beta_K} \quad (2)$$

\bar{P}_{out} here is 2.75MW, while β_{new} is 0.33.

W-Band Klystron Design

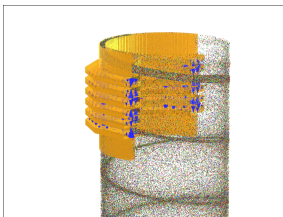
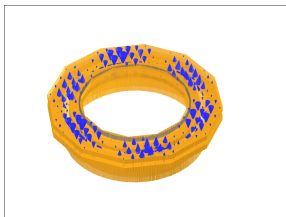
important parameters

- **resonant frequency of the input and idler cavities:** 30 GHz
- **resonant frequency of the output cavity:** 90 GHz
- **mode in the input and idler cavity:** TM_{110} -mode
- **mode in the output cavity:** TM_{310} -mode
- **beam velocity:** $0.412 \cdot c_0$
- **beam voltage:** 50 kV
- **beam power:** 50 kW

W-Band Klystron Design

output cavity

- output cavity in prism form with 12 edges
- tuning ring instead of output waveguides
- modulation depth of beam is 5%
- coupled gap cavity in π -mode



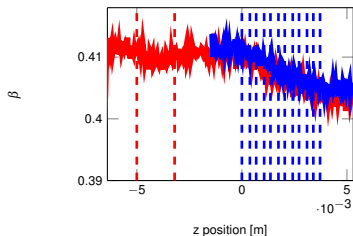
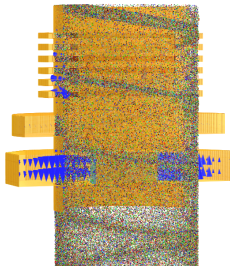
cavity	$\overline{P}_{out}/\overline{P}_{in}$ [%]
two gaps	0.8%
four gaps	1.32%
six gaps	1.986%

W-Band Klystron Design

output cavity

- Output cavity with "penultimate" cavity

the "next to the last" cavity, operates in TM_{110} -mode, inductively excited, improves the bunch quality



output efficiency of six gap cavity with penultimate: 2.36%

W-Band Klystron Design

Idler Cavity

- improve the gain of the klystron
- inductively excited for modulation enhancement

$$\Phi = \tan^{-1} \left(\frac{\omega_0^2 - \omega^2}{\omega_0 \omega / Q} \right) \quad (3)$$

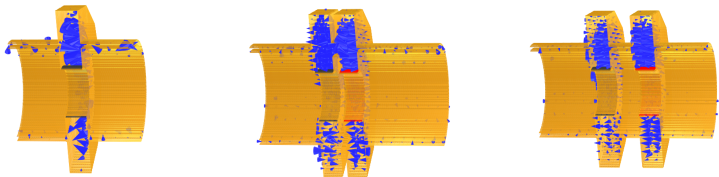
Beam under Investigation with initial modulation depth of 1%

Φ	modulation depth [%]	power loss [%]
65°	2.3543	0.025
70°	2.1359	0.016
75°	1.8689	0.009
80°	1.6504	0.006
85°	1.3592	0.002

W-Band Klystron Design

Idler Cavity

- Three Idler Types:
Single Idler , Coupled Idler and Clustered (but not Coupled) Idler



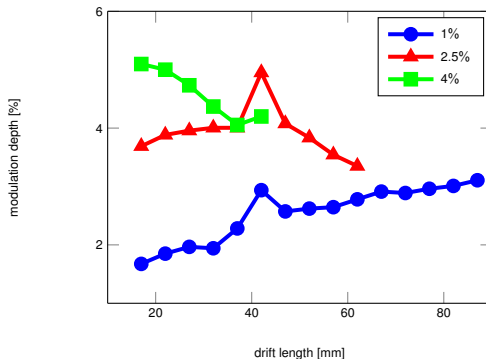
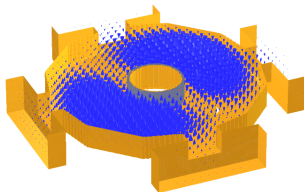
$$\Phi = 80^\circ, Q = 1000, \text{ modulation depth}=1\%$$

idler type	modulation depth in %
one single cavity with Q	1.65
coupled cavities with half Q	1.38
clustered cavities with half Q	1.58
clustered cavities with Q	2.67

W-Band Klystron Design

Input Cavity and Drift Length of Electron Beam

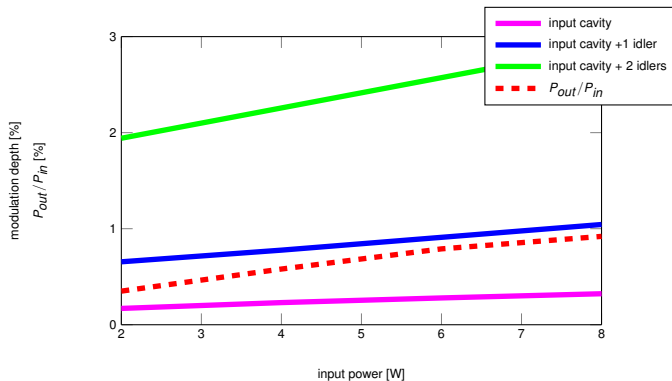
- input cavity in TM_{110} -mode with four power feeding waveguides
- after different drift lengths electron beam with initial modulation depth of 1%, 2.5% and 4% achieve different new depths in clustered idler



W-Band Klystron Design

Linearity of Klystron

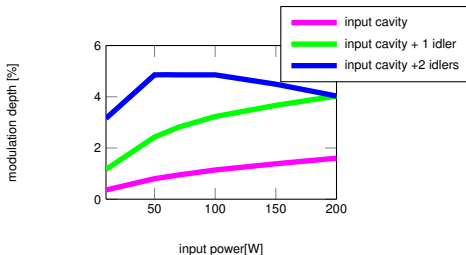
– linear area



W-Band Klystron Design

Linearity of Klystron

- non-linear / saturation area



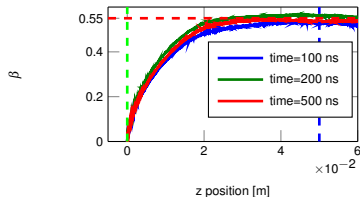
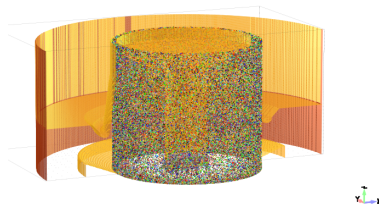
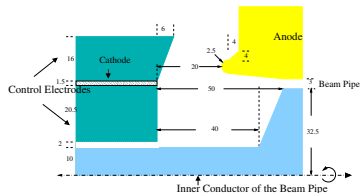
Power Recovery

overall efficiency of this klystron

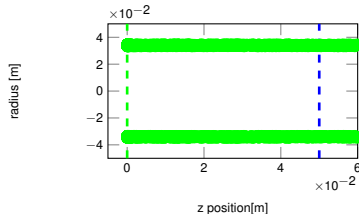
$$\eta_{ov} = \frac{\overline{P}_{out}}{\overline{P}_{in} - \overline{P}_{rec}} = 10.4\% \quad (4)$$

Electron Gun for Generating a Hollow Beam

Electron Gun for Non-compressed Beam



Normalized electron velocity as a function of longitudinal distance z for different calculation times

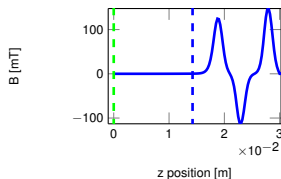
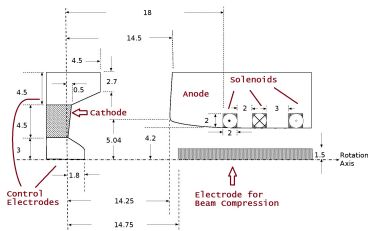


distribution in the electron gun

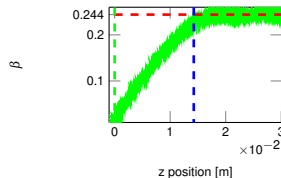
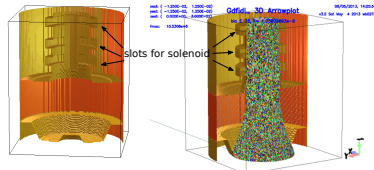
Electron

Electron Gun for Generating a Hollow Beam

Electron Gun for Compressed Beam



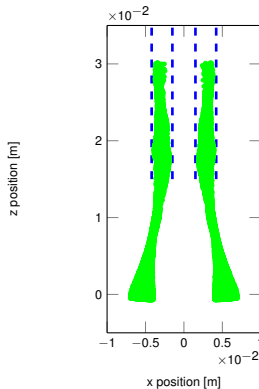
Magnetic flux in z direction at radius of 2.85mm



Velocity of electrons in longitudinal direction continuously increases in the electron gun

Electron Gun for Generating a Hollow Beam

Electron Gun for Compressed Beam



Cross-section of electron beam in the electron gun with convergent trajectory; the beam pipe is marked with dashed blue lines

Conclusions

- **Chances**

- great potential of power amplification up to MW
 - linearity in known area
 - easy to manufacture

- **Challenges**

- realisation of electron gun for compressed beam
 - stability under high power

○ This project is founded by Deutsche Forschungsgesellschaft.