

THALES

Work function of dispenser cathodes and life prediction model

VDE-ITG CONFERENCE BAD-HONNEF 5-6/09/2018
L1. 1-2

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OUTLINE

- Presentation of Thales AVS FR in Vélizy France
- Impregnated cathode description
- Characterization of cathodes (physical and chemical)
- Model of dispenser cathodes
- Model vs. Experimental results

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TAVS in Vélizy France

➤ Design and production of Traveling Wave Tubes, klystrons, gyrotrons, generators, space amplifiers, defense transmitters, energy storage...



KLYSTRON MULTI FAISCEAUX



KLYSTRON



KLYSTRON



SPACE AMPLIFIER



TRANSMITTER FOR RADAR



GYROTRON

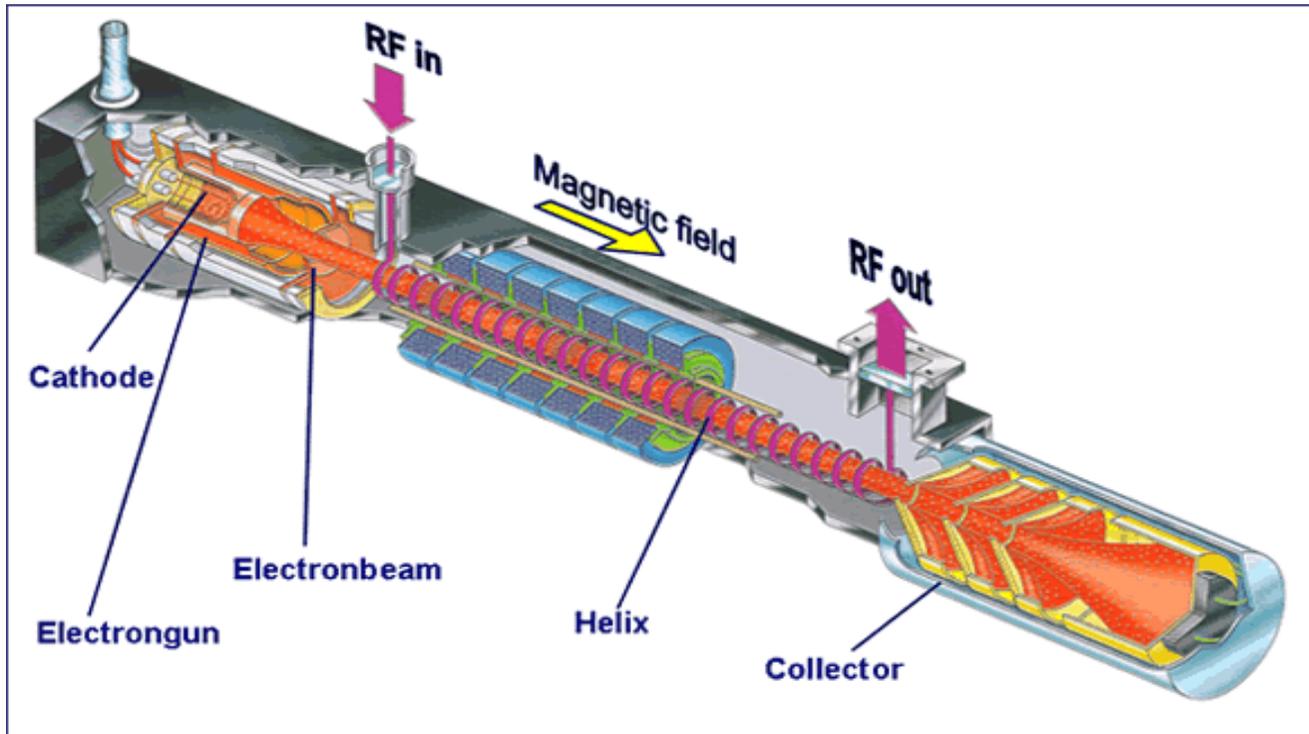


WORLD #1 FOR SPACE AND SCIENCE TUBES
EUROPEAN #1 FOR TELECOM AND DEFENSE TUBES

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Cathodes in TWT's



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Helix TWT with impregnated cathode

Cathodes in Orbit: reliability considerations

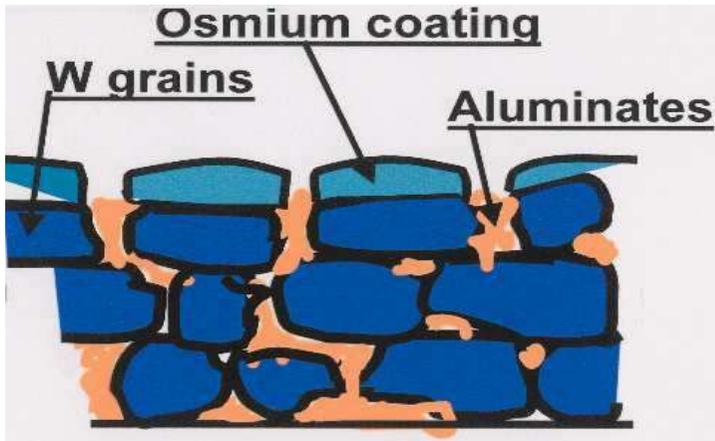
Cathodes in Orbit Long life (15 years) required !!!

- Reliability considerations
 - Cathode characterization
 - On-ground Life-tests
 - Model of life prediction

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Impregnated cathode description

Cathodes in use at TAVS:

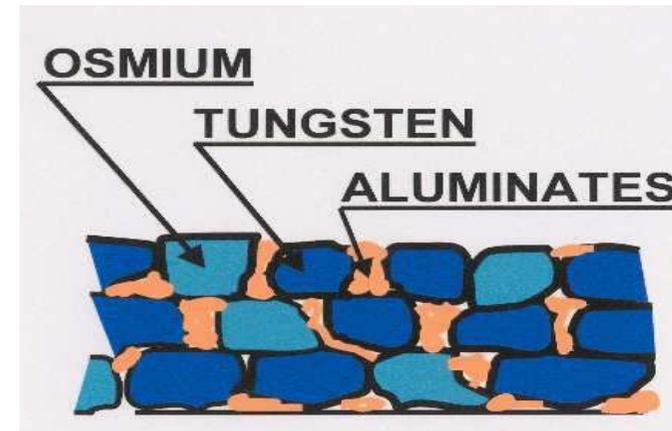


M-type cathode

**Porous tungsten pellet
(porosity 18 %)
Impregnated with barium, calcium
aluminates
Osmium or Os-Ru coated (0.5 μm)**

MM-Type cathode

**Porous tungsten-osmium pellet
Impregnated with barium,
calcium aluminates**



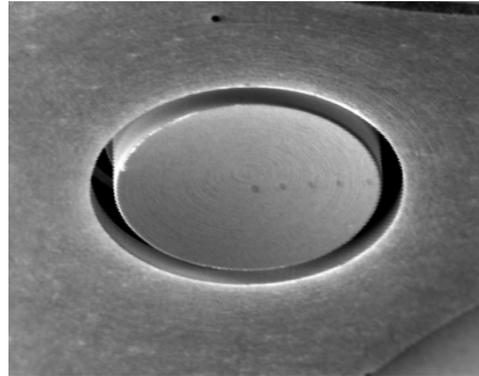
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Characterization of cathodes (physical and chemical)

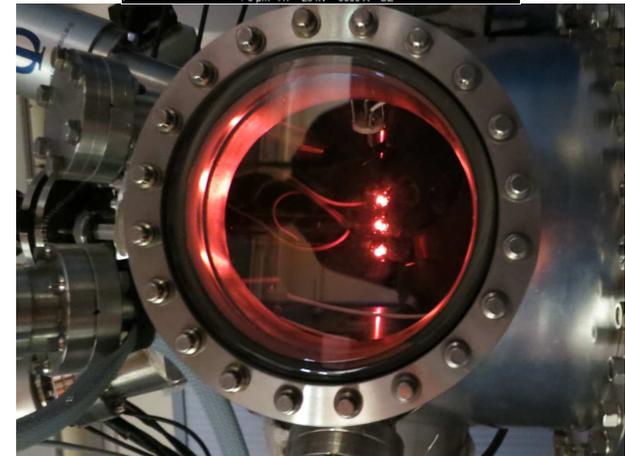
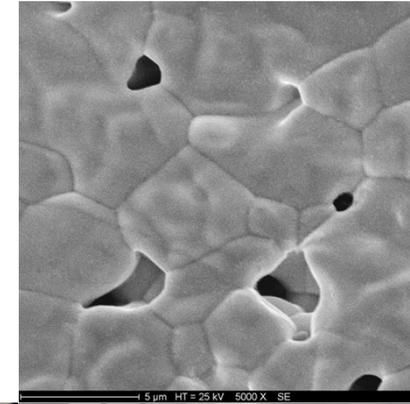
Auger spectroscopy



Phoibos spectrometer from SPECS GmbH



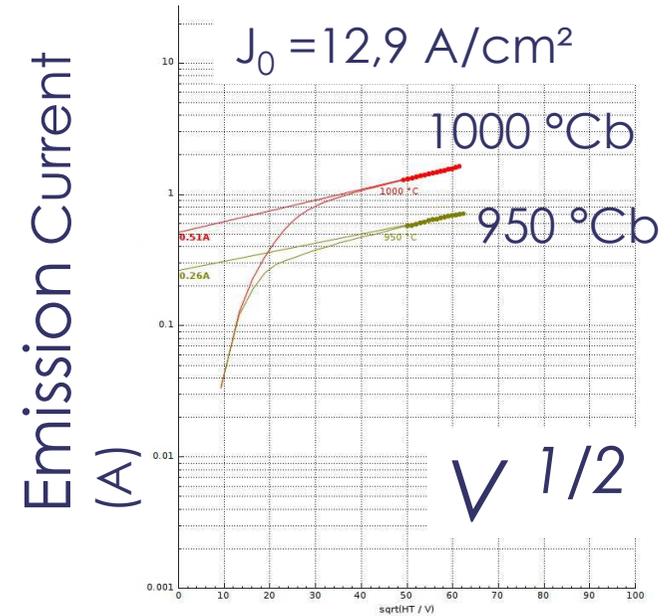
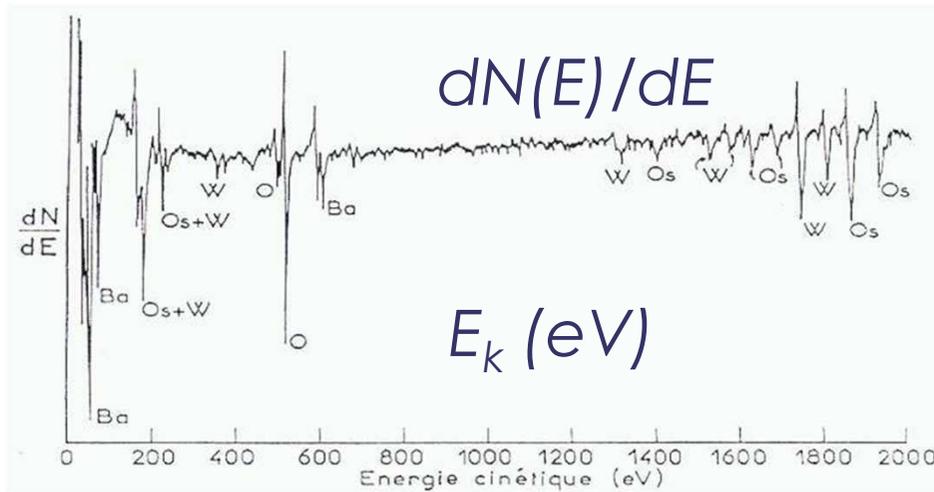
In situ image of cathode by SED: e spots by « carbon pinning »



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Characterization of cathodes (physical and chemical)

- Auger spectroscopy combined with in-situ emission meas't (J_0)
- Only Ba, O, W and Os detected on cathode surface after activation
- Selection of « Best in class cath. »

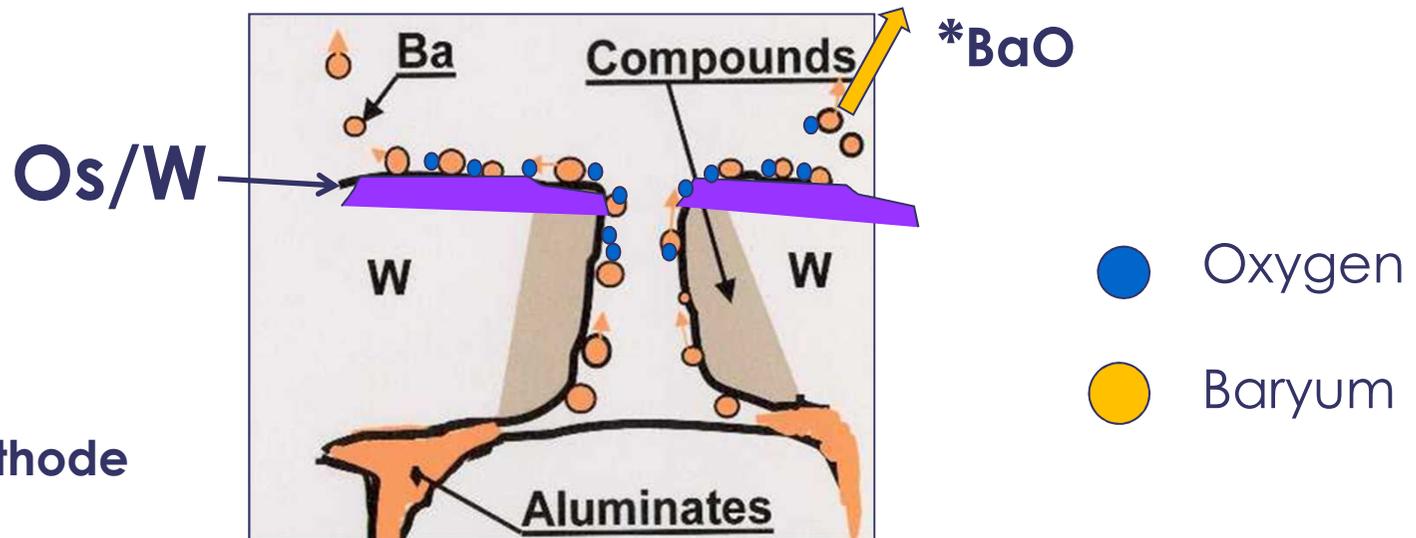


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Model of dispenser cathode

Chemical reactions inside the pores, Ba and O transport over the W surface

Build-up of 1 monolayer ($\theta = 1$) or sub-monolayer ($\theta < 1$) of Ba-O

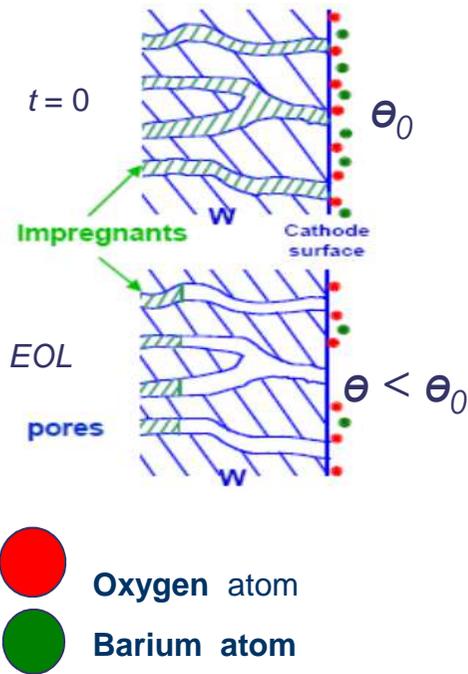


M-type cathode

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Model of dispenser cathodes

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LIFETIME MODEL COMMON BASIS: The study on dispenser cathode life of Longo (Hugues Aircraft) shows a trend of emission slump

$$* \Delta J_n \sim t^{1/2}$$

His life model is based on calculation of Ba coverage θ variation with time.

The trend $\Delta J_n \sim t^{1/2}$ has been confirmed by several authors:

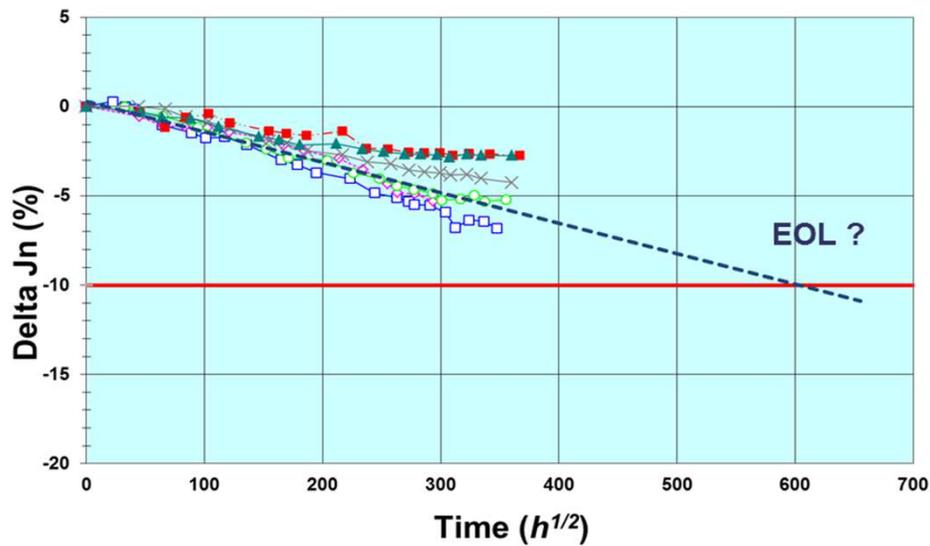
- **Mita**(NEC), **Higuchi** (Toshiba), **Shroff**(Thales)

* J_n = cathode operating current density in tube

Model of dispenser cathodes

Decrease of nominal current of the cathodes with time

- $\Delta J_n \sim t^{1/2}$ trend verified on TWT's at Thales
- Can we extrapolate the trend to determine the End Of Life?



20 W -Ku :

- $J_n = 0,7 \text{ A/cm}^2$
- $T = 1010 \text{ }^\circ\text{C}_B$

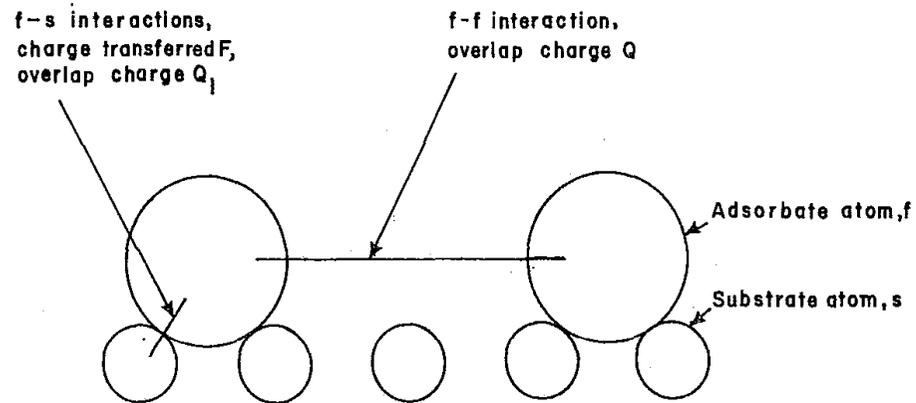
Model of dispenser cathodes

The different bricks to build the cathode lifetime model used in * Thales

Brick 1: Longo and Vaughan :

$$\frac{1}{(J_n)^n} = \frac{1}{(J_{SC})^n} + \frac{1}{(J_{TL})^n}$$

Brick 2: Gyftopoulos & Steiner:



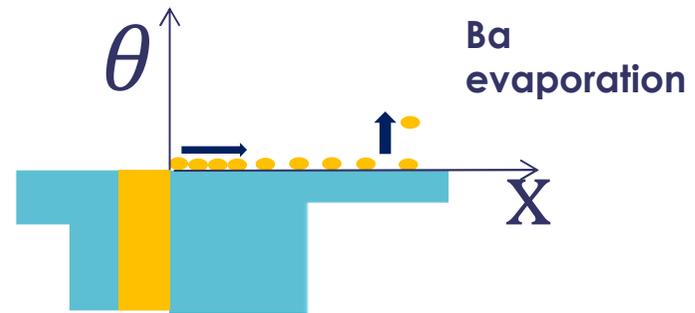
* A.M. Shroff model

Model of dispenser cathodes

The different bricks to build the model of Shroff

Brick 3: Fote & Luey

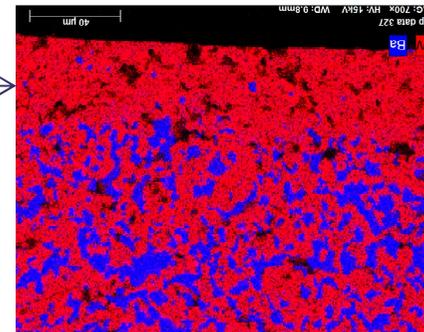
Fraction of Ba monolayer θ as a function of distance from the matrix pore



Brick 4: Shroff study of Ba depletion

Zone of empty pores

Ba image by EDX (blue)



Cross section

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Model of dispenser cathodes

Brick 1: Longo-Vaughan

Cathode nominal current J_n can be calculated using the **LONGO-VAUGHAN** equation

$$\frac{1}{(J_n)^n} = \frac{1}{(J_{SC})^n} + \frac{1}{(J_{TL})^n}$$

- > J_n : operating current density of the cathode in the tube
- > J_{sc} : current density of the cathode in space charge regime
- > J_{TL} : *current density of the cathode in temperature-limited regime ($\sim J_0$).
- > n : Vaughan exponent between 1 and 6

Model of dispenser cathodes

Brick 2: Gyftopoulos & Steiner

$$\Phi(\theta) = \Phi_s + CQ(\theta) + bF(\theta)$$

$$\Phi(\theta) = \Phi_s - (\Phi_s - \Phi_f)M(\theta) + bF(\theta)$$

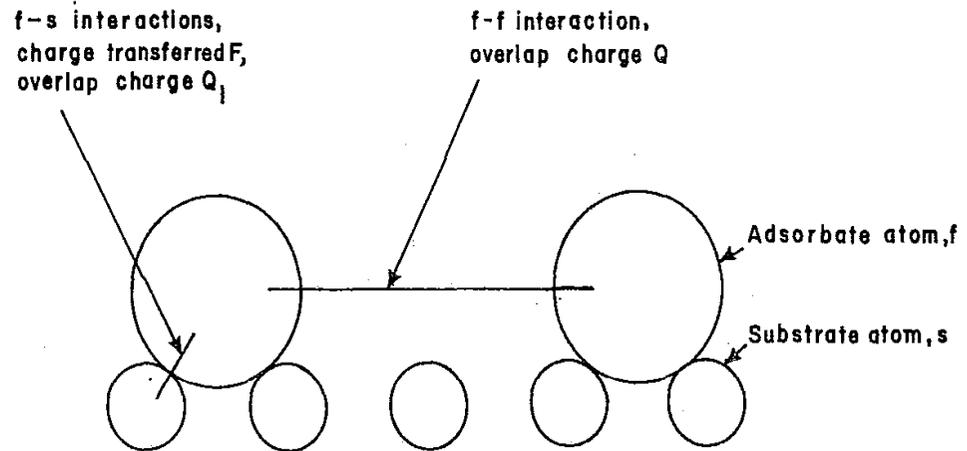
Φ_s : substrate work function

$CQ(\theta)$: covalent contribution

$bF(\theta)$: dipole moment

Φ_f : film work function

$M(\theta)$: Morse function ($M(1) = 1; M(0) = 0$)



Model of dispenser cathodes

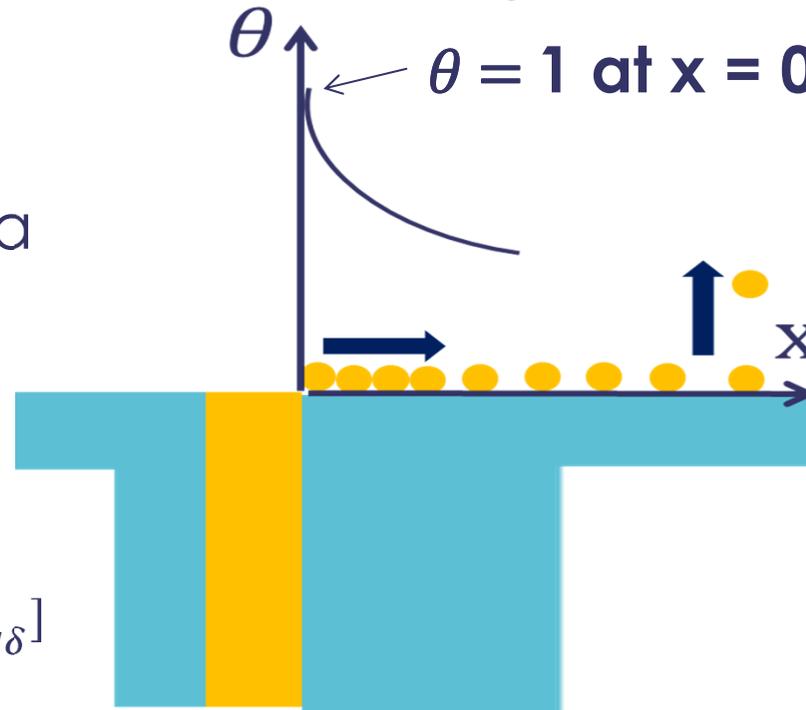
Brick 3: Fote and Luey: transport of Ba over the emitting face

→ θ as a function of distance x from the Ba source

$$D \frac{d^2\theta}{dx^2} = \frac{\theta^v}{\tau}$$

$$L_\delta = (D \cdot \tau)^{1/2}$$

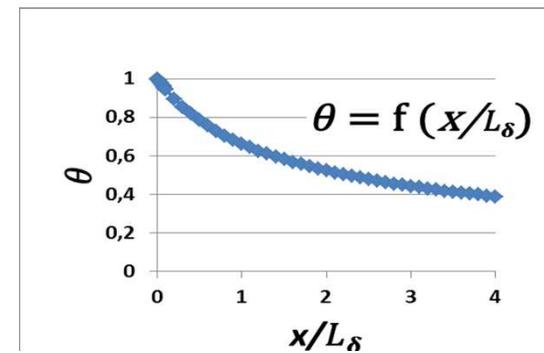
$$L_{\delta(cm)} = 8 \cdot 10^{-5} \cdot e^{\left[\frac{11600}{T} V_{L\delta}\right]}$$



Model of dispenser cathodes

Fote & Luey unidimensional model: θ as a function of distance from the Ba source scaled to L_δ

$$\theta_x = \left[1 + \frac{\nu - 1}{\sqrt{2(\nu + 1)}} \cdot \frac{x}{L_\delta} \right]^{-2 / (\nu - 1)}$$



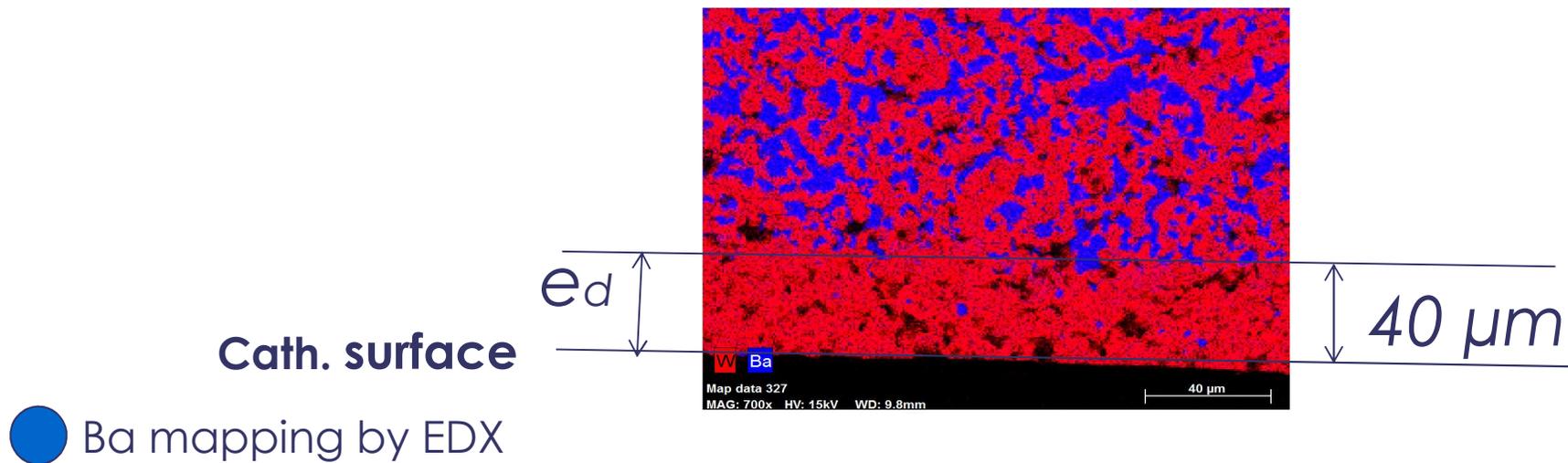
L_δ is the "effective diffusion length" over which emission is space charge limited (slotted pore geometry)

At $x = L_\delta$ the value of θ is 0,67 (i.e $\frac{2}{3}$ of ML)

Model of dispenser cathodes

Brick 4: Schroff's study of Ba depletion

- Ba depletion e_d measured by EDX
- On real cathodes in diodes at different intervals of time and temperature



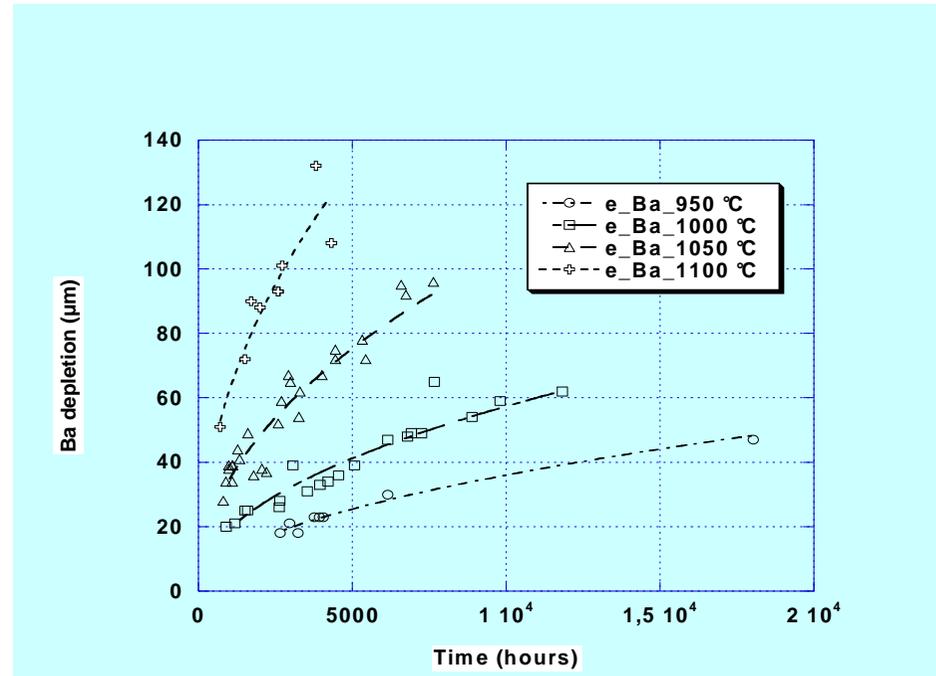
Model of dispenser cathodes

Ba depletion depth with time (experimental)

$$e(t, T) = A_{II} \cdot t^{1/2} \cdot e^{\left[\frac{-11600}{T} \left(\frac{V_e}{2} \right) \right]}$$

V_e : activation energy of
the depletion deduced from experiment

**Depletion measurements
presented by J.M. Roquais *et al.*
IVESC 2002 in Saratov**



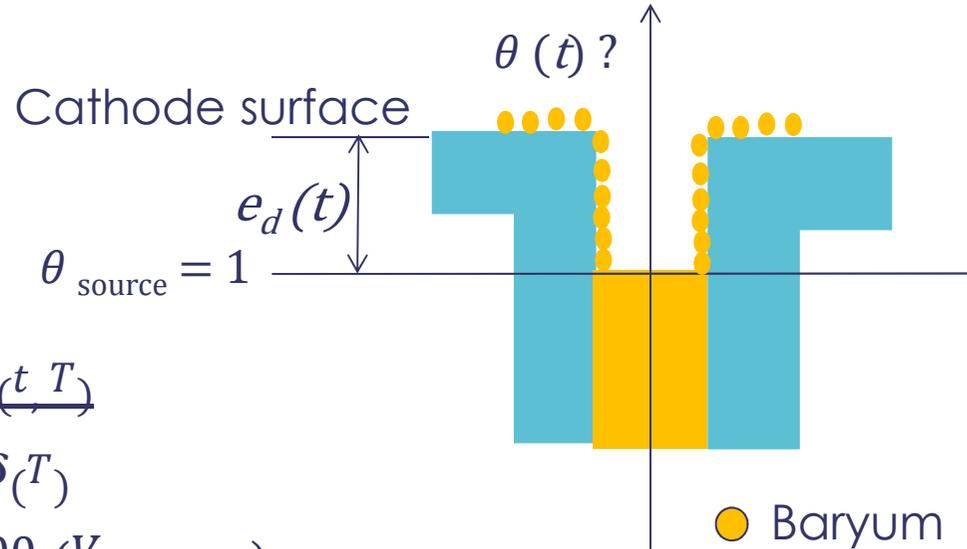
Model of dispenser cathodes

Shroff 's model:
surface diffusion inside
the pores (unidimensional)

$$\theta(t, T) = 1 - \sqrt{2/\nu + 1} \cdot \frac{e_d(t, T)}{L_{\delta}(T)}$$

$$\Delta\theta(t, T) = -\alpha \cdot t^{1/2} \cdot e^{\left[\frac{-11600}{T} \left(\frac{V_{ed}}{2} + V_{L\delta} \right) \right]}$$

$$V_{\theta}(eV) = \left(\frac{V_{ed}}{2} + V_{L\delta} \right) \quad 2,1 < V_{\theta} < 2,4$$



Model of dispenser cathodes

- Saturation and space charge currents can be calculated at any time with following approximations:

- $J_0(t, T) = f(\Phi) = f(\theta)$

- $J_{sc}(t, T) = J_{sc}(t=0) \cdot \theta(t) / \theta_0$

Calculation of J_{sc} and J_s evolution with time $\rightarrow J_n$ vs time

$$\frac{1}{(J_n)^n}(t) = \frac{1}{(J_{sc})^n}(t) + \frac{1}{(J_0)^n}(t)$$

Model vs. Experimental results

Available experimental data

- J_0 as a function of time (measured in **bulbs in diode configuration**)
- J_n as a function of time measured in **TWT's** and **Test vehicles (TV's)**

Calculation method (Excel)

- Parameters initially set (for M-type cathode):
 - Temperature: T = life-test operating temperature
 - $J_0 (t=0) = 11 \text{ A/cm}^2$ at $1000 \text{ }^\circ\text{C}$
- Adjustable parameters :
 - V_θ : Activation energy of θ
 - initial coverage θ_0 : 0,8 -1,0

Model vs. Experimental results

Gyftopoulos & Steiner applied to our M-type cathode

$$\Phi(\theta) = \Phi_s + CQ(\theta) + bF(\theta)$$

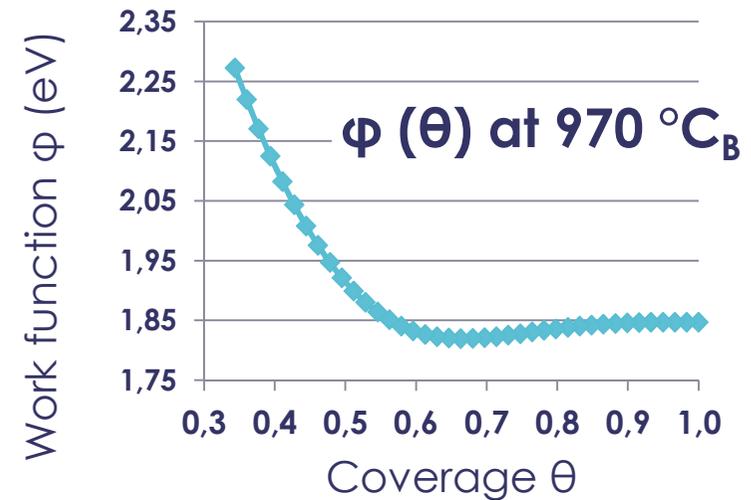
$$\Phi(\theta) = \Phi_s - (\Phi_s - \Phi_f)M(\theta) + bF(\theta)$$

Φ_s : substrate work function (W-Os)

Φ_f : film work function (exp. values)

$CQ(\theta)$: covalent contribution (G-S calc.)

$bF(\theta)$: dipole moment (G-S calc.)



Minimum of $\Phi(\theta)$ occurs for $\theta \sim 2/3$

Model vs. Experimental results

J_0 vs. Time : comparison of our model with meas. in diodes at 1000 °C_B

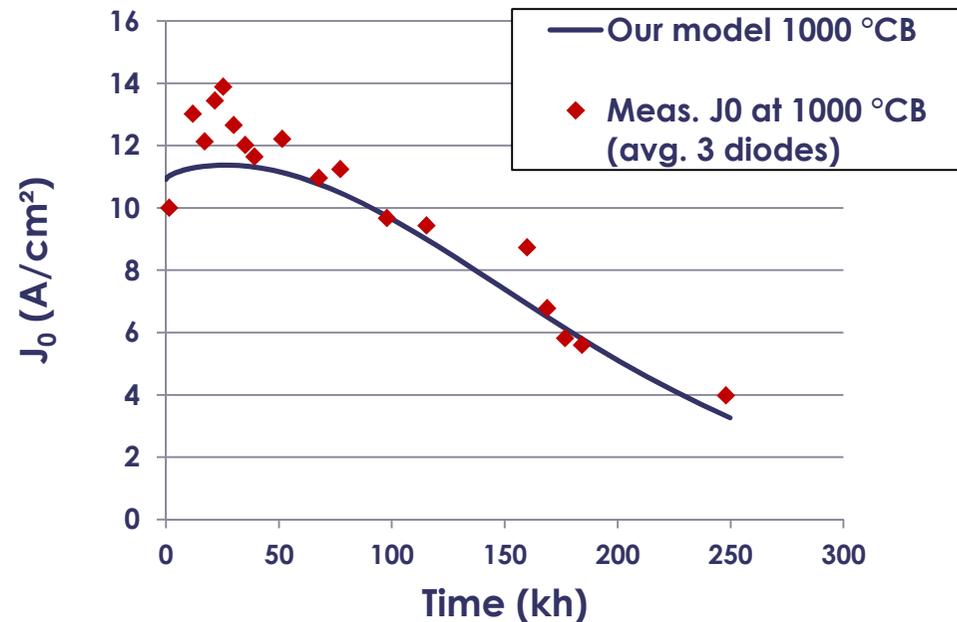
Calculation at 1000 °C_B:

$$\theta_{(t)} \Rightarrow \varphi_{(t)} \Rightarrow * J_{0(t)}$$

With:

$$\theta_0 = 0,8$$

$$V_\theta = 2,13 \text{ eV (Schroff's value)}$$



* J_0 calculated using the Richardson-Dushman equation

Model vs. Experimental results

J_0 vs. Time : comparison of our model with meas. in diodes at 1030 °C_B

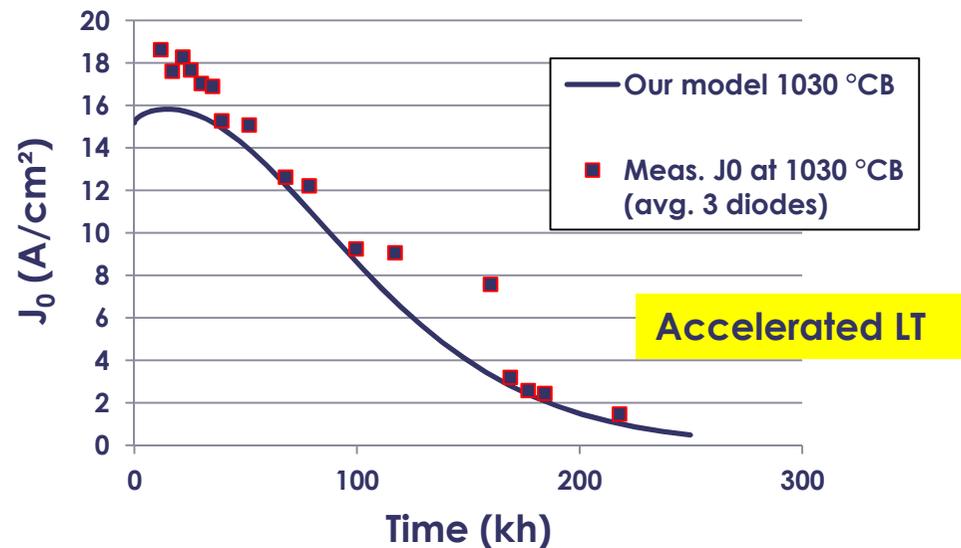
Calculation at 1030 °C_B:

$$\theta_{(t)} \Rightarrow \varphi_{(t)} \Rightarrow J_{0(t)}$$

With:

$$\theta_0 = 0,8 \text{ (best fit)}$$

$$V_\theta = 2,13 \text{ eV (Schroff's value)}$$



The good fit at 1000 and 1030 °C_B validates our calculation of $\theta(t)$ and $\varphi(t)$

Model vs. Experimental results

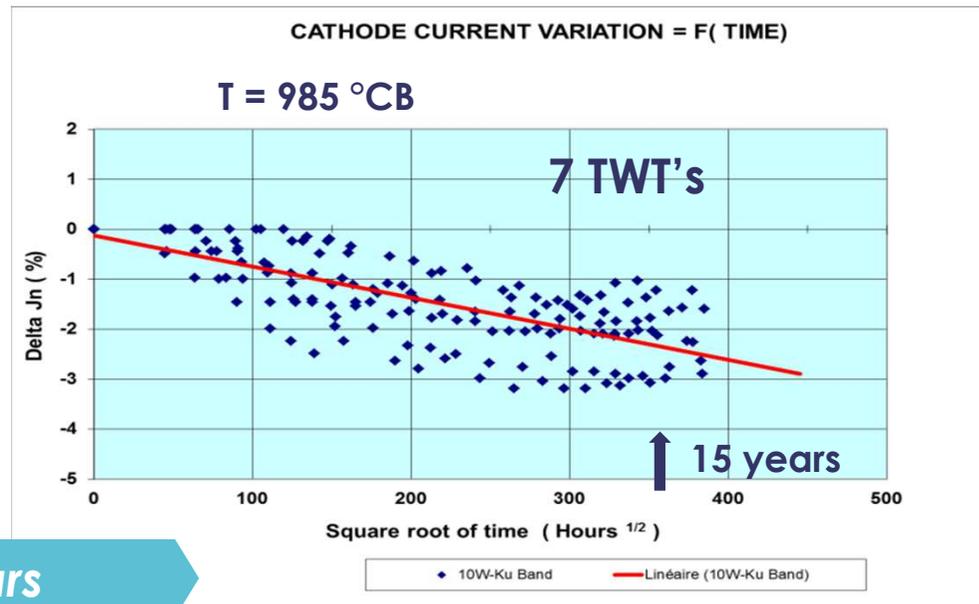
Calibration of $\Delta\theta(t, T)$ using experimental data of tubes life-test

V_θ adjusted to match emission decay in TWT's

$$\Delta\theta(t, T) = -\alpha \cdot t^{1/2} \cdot e^{\left[\frac{-11600}{T} V_\theta\right]}$$

$$\Delta J_{SC}(t, T) / J_{SC0} = \Delta\theta(t, T) / \theta_0$$

$$V_\theta \sim 2,13 \text{ eV} + \Delta V_\theta$$



Decay is only ~3% after 15 years

Model vs. Experimental results

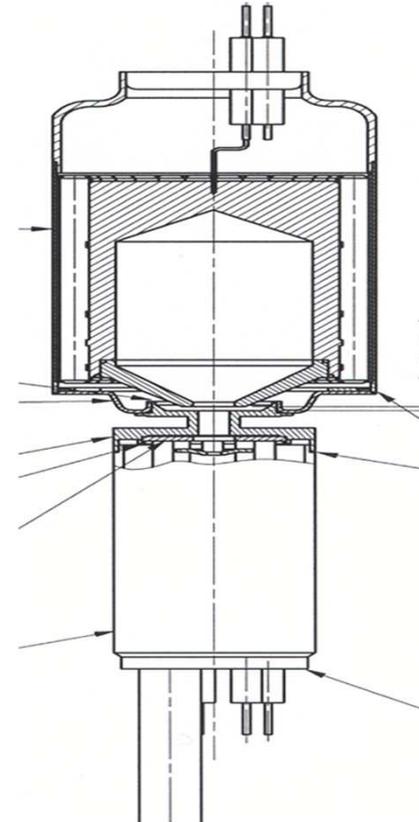
Test vehicle: gun/collector

Conditions

- No microwave signal
- 3 x TV's in life at 2 different T°C:
 - 985 °CB (2 TV's)
 - 1045 °CB (1 TV): accelerated LT

Measurements

- Jn vs. time



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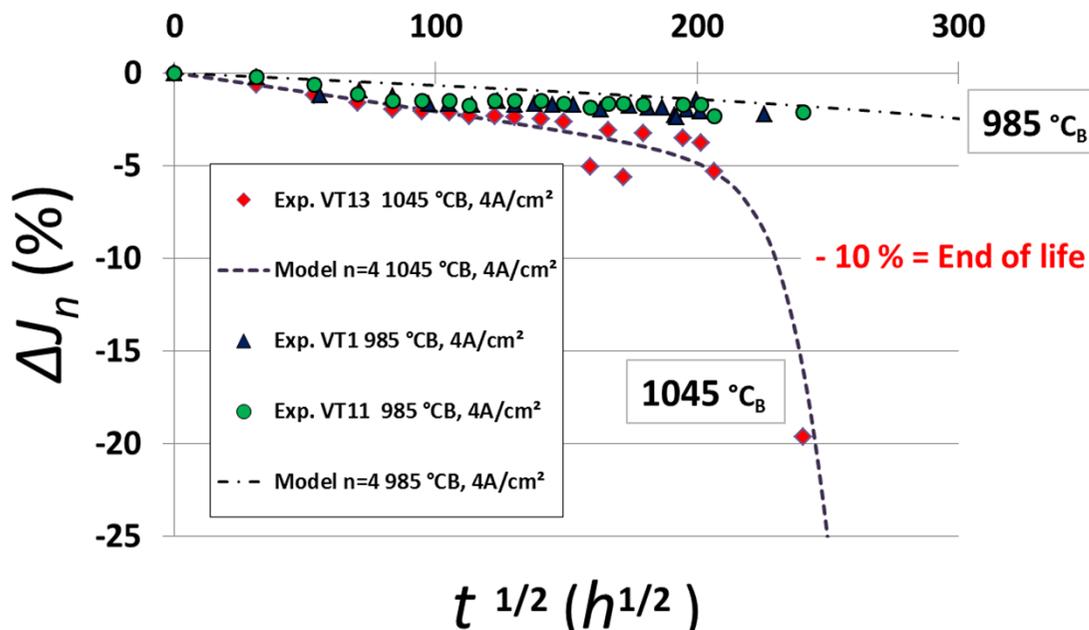
Model vs. Experimental results

Gun/collector vehicle

$J_n (t=0) = 4 \text{ A/cm}^2$

1 VT at 1045°C_B

2 VT's at 985°C_B



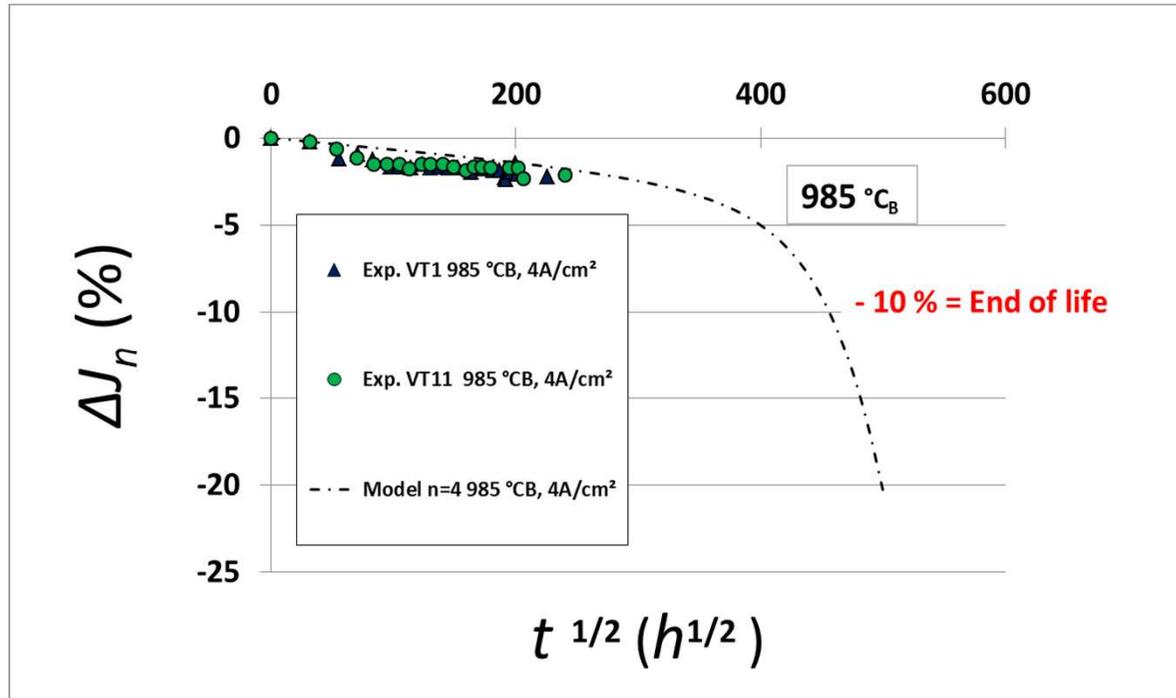
Model describes well experimental results. J_n departs from $t^{1/2}$ law at 1045°C_B at $t \sim 40 \text{ kh}$.

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Model vs. Experimental results

Projection of lifetime
with model

$$J_n(t=0) = 4 \text{ A/cm}^2$$



Projected EOL > 160 000 h at 985°C_B for $J_n = 4 \text{ A/cm}$

Long-term LT: Prediction

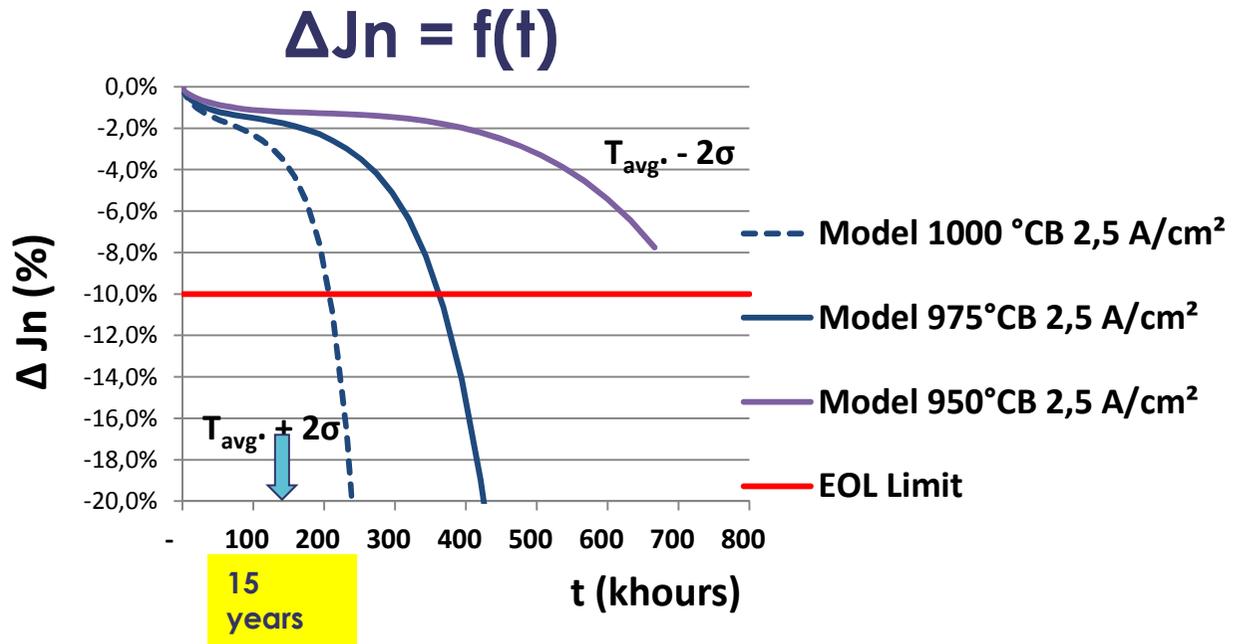
Prediction of cathode life in Tubes

$J_n(t = 0) = 2,5 \text{ A/cm}^2$

$T_{avg.} = 975 \text{ } ^\circ\text{C}_B$

Calculation at:

- $T_{avg.} + 2\sigma$
- $T_{avg.}$
- $T_{avg.} - 2\sigma$



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CONCLUSION

As a summary on the Long-term life tests and model:

Experimental:

- In diodes, the M-type cathodes are still capable of $J_0 = 8\text{A/cm}^2$ after 15 years at $1000\text{ }^\circ\text{C}_B$
- In TWT's at $0,6\text{ A/cm}^2$, $\Delta J_n \sim -3\%$ after 15 years at 985°C_B

Model/ lifetime calculation :

- The long-term data have allowed to adjust the model parameters
- The law of variation of J_n is well predicted by the lifetime model **including the final abrupt decay observed in accelerated lifetests**
- For $975\text{ }^\circ\text{C}_B$ at $2,5\text{ A/cm}^2$, or $985\text{ }^\circ\text{C}_B$ at 4 A/cm^2 **the cathode lifetime exceeds clearly 15 years**

Thank you for your attention !!

Long-term LT: Prediction

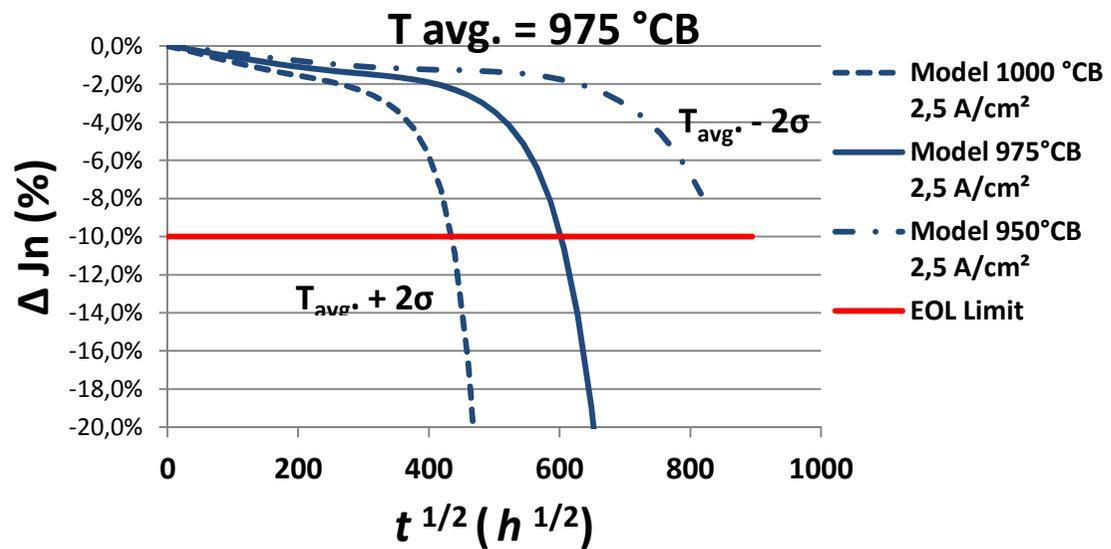
Prediction of cathode life in Tubes

$J_n(t = 0) = 2,5 \text{ A/cm}^2$

Calculation at:

- $T_{avg.} + 2\sigma$
- $T_{avg.}$
- $T_{avg.} - 2\sigma$

$\Delta J_n = f(t^{1/2})$



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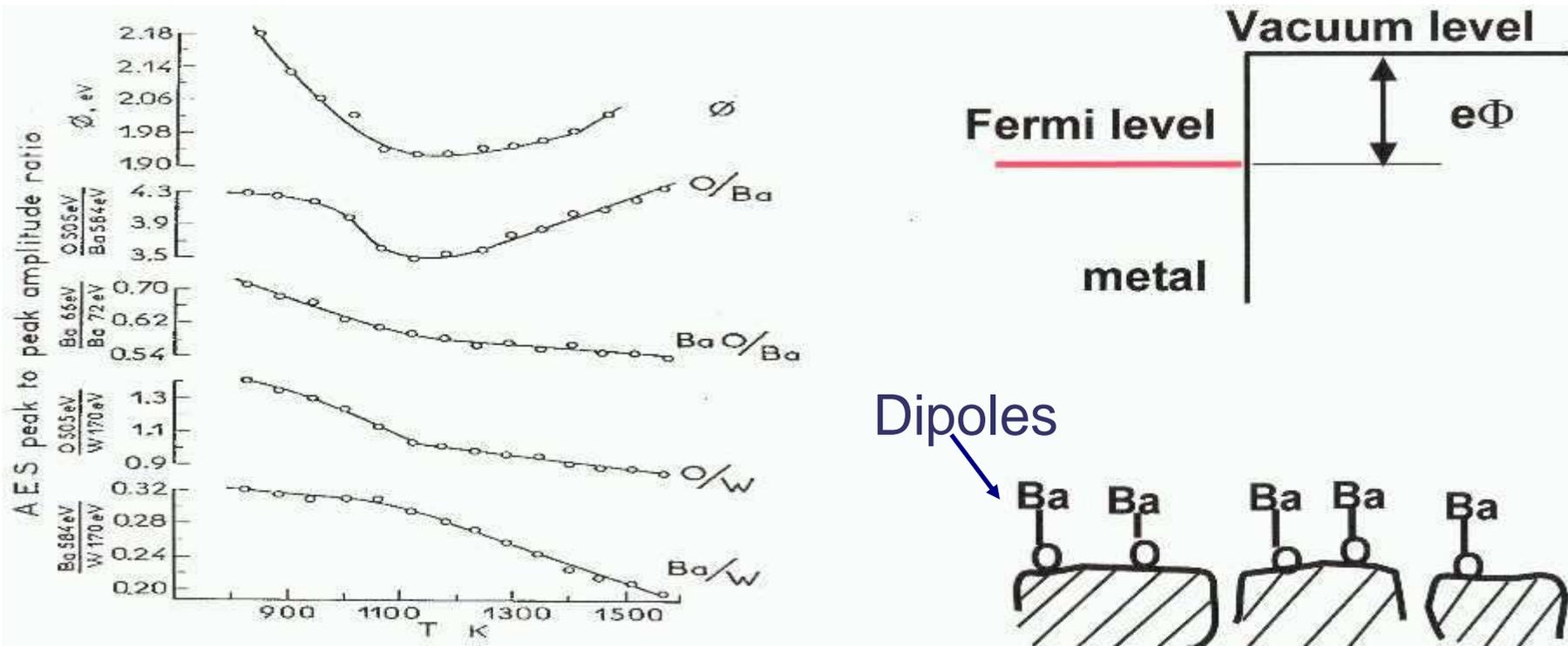


Back-up

Characterization of cathodes (physical and chemical)

Evolution vs. temperature of Auger peaks (Ba/W, O/Ba,.....) correlated with work function Φ for an S-type cathode (D. Brion et al.)

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Different types of thermionic cathodes and their application

Design cathodes MBK (Multi-Beam Klystron), 7 cathodes

Ex: TH1802 (1.3GHz)

- cathodes M (4.1.1)
- $I_k = 135 \text{ A}$ (5 A/cm^2),
- $T_k = 1010 \text{ }^\circ\text{C}$
- Lifetime $\sim 60\,000$ Hours



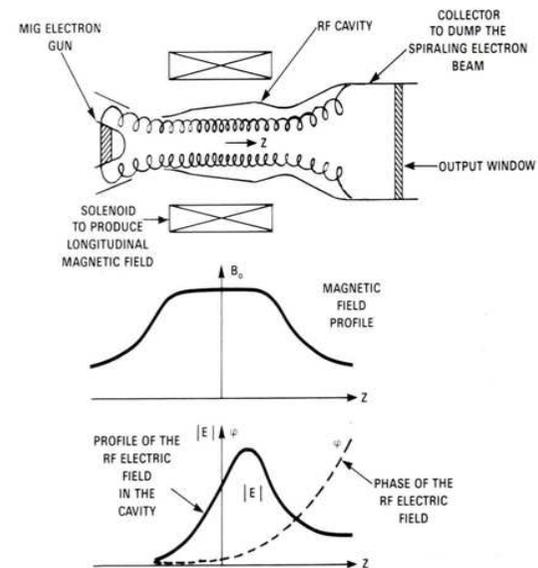
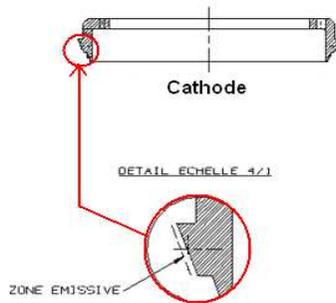
Cathode loading = 5.0 A/cm^2

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Different types of thermionic cathodes and their application

Design cathode Gyrotron

Ex: TH1507 (140Ghz) - Cathode S (4.1.1) $I_k=40A$
(2,5 A/cm²; T.L. réaime) $T_k = 900-950$ °Cb



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Different types of thermionic cathodes and their application

TED GYROTRON : TH1507

Application : Thermonuclear fusion
(Stellarator W 7-X Germany)

- Frequency : 140 GHz
- Output power : 1MW CW
- 45 % efficiency

- S type cathode 4.1.1.
- $I_k = 42 \text{ A}$
- $J_k = 2.4 \text{ A/cm}^2$
- $T_k = 900\text{-}950 \text{ }^\circ\text{C}$ (TL regime)
- required cathode life time: 50000 Hrs

