

# Considerations for the dual-frequency operation of 140 GHz Megawatt-class W7-X gyrotrons at 175 GHz for CTS plasma diagnostics

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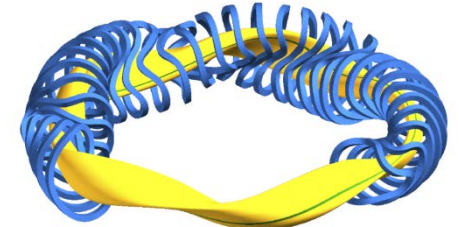
- Motivation
- Structure of the W7-X Gyrotron
- Window and Quasi-Optical System
- Electron Gun
- Cavity
- Conclusion & Outlook

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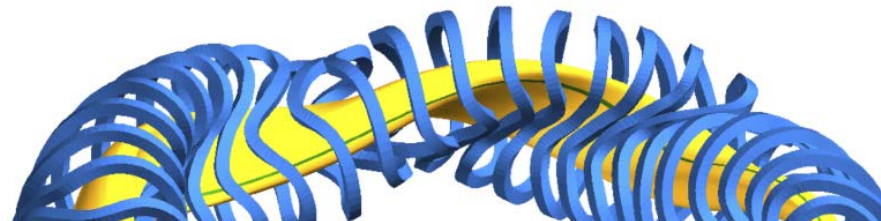
# Wendelstein 7-X (W7-X)

- Stellarator W7-X is an experimental reactor to demonstrate fusion relevant plasma performance
- **Heating** of the plasma through Electron Cyclotron Resonance Heating



➔ 10 **gyrotr**

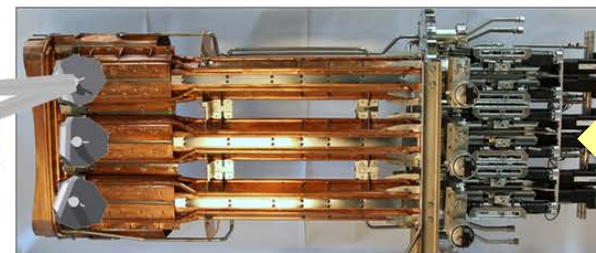
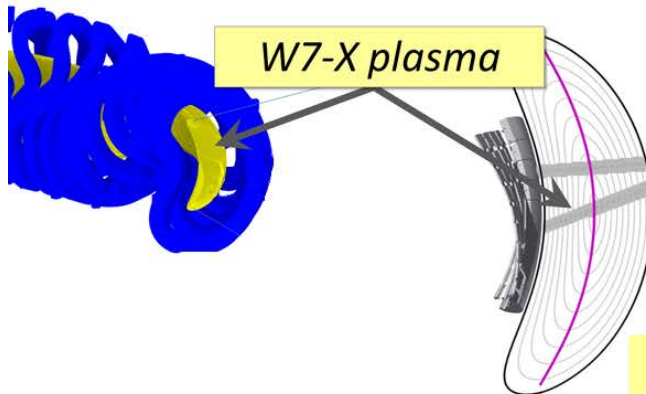
- Gyrotrons oper



on **resonance**

*Gyrotron*

*W7-X plasma*



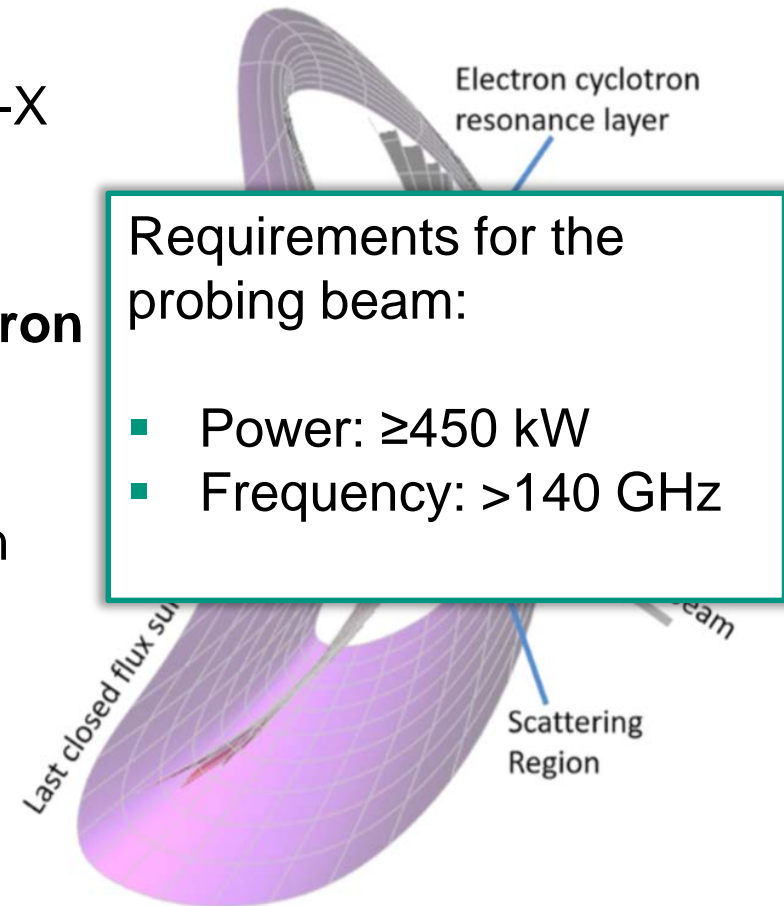
*launcher mirrors*

*Quasi-optical transmission*



# Collective Thomson Scattering (CTS)

- CTS diagnostic of the plasma:  
Measurement of ion temperature at W7-X
- Probing beam needs high power  
Source at W7-X: **140 GHz ECRH gyrotron**
- **Absorption of 140 GHz wave**  
  - ➔ measurement in electron cyclotron resonance layer not possible
- Refractions in plasma at lower frequencies  
  - ➔ **higher frequency** for CTS at W7-X needed



Requirements for the probing beam:

- Power:  $\geq 450$  kW
- Frequency:  $> 140$  GHz

# Motivation

Is it possible to operate the **existing 140 GHz gyrotron** at a **higher frequency**?

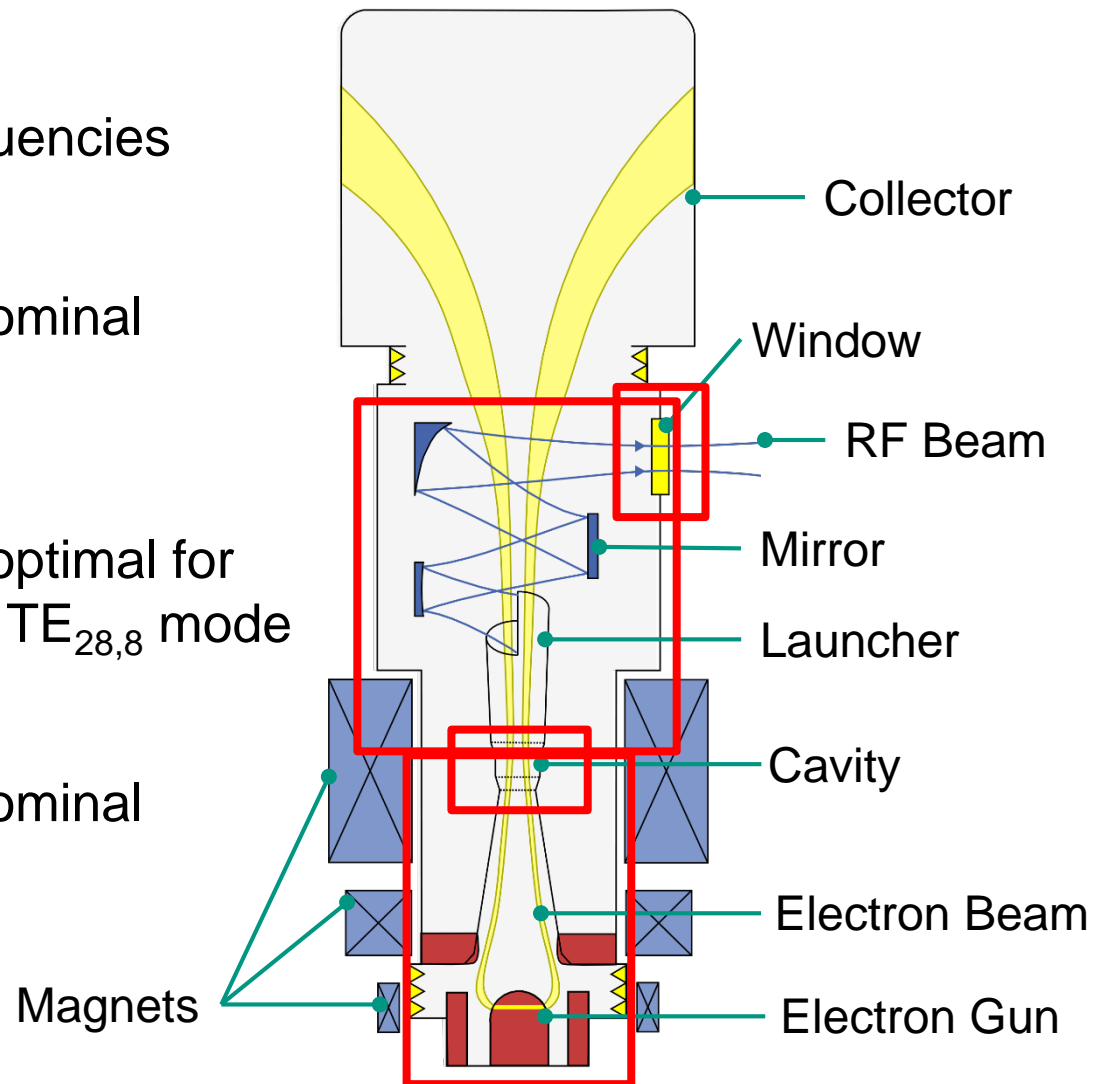
- Operation of a gyrotron at a different frequency is not straightforward
  - ➔ W7-X gyrotron was designed and optimized specifically for 140 GHz
- Operation at a different frequency requires **investigation of the subcomponents** of the gyrotron

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# Structure of the 140 GHz W7-X Gyrotron

- Window transparency
  - ➔ limits possible frequencies
- Quasi-optical system
  - ➔ optimized for the nominal  $TE_{28,8}$  mode
- Electron gun
  - ➔ Beam parameters optimal for interaction with the  $TE_{28,8}$  mode
- Cavity
  - ➔ optimized for the nominal  $TE_{28,8}$  mode





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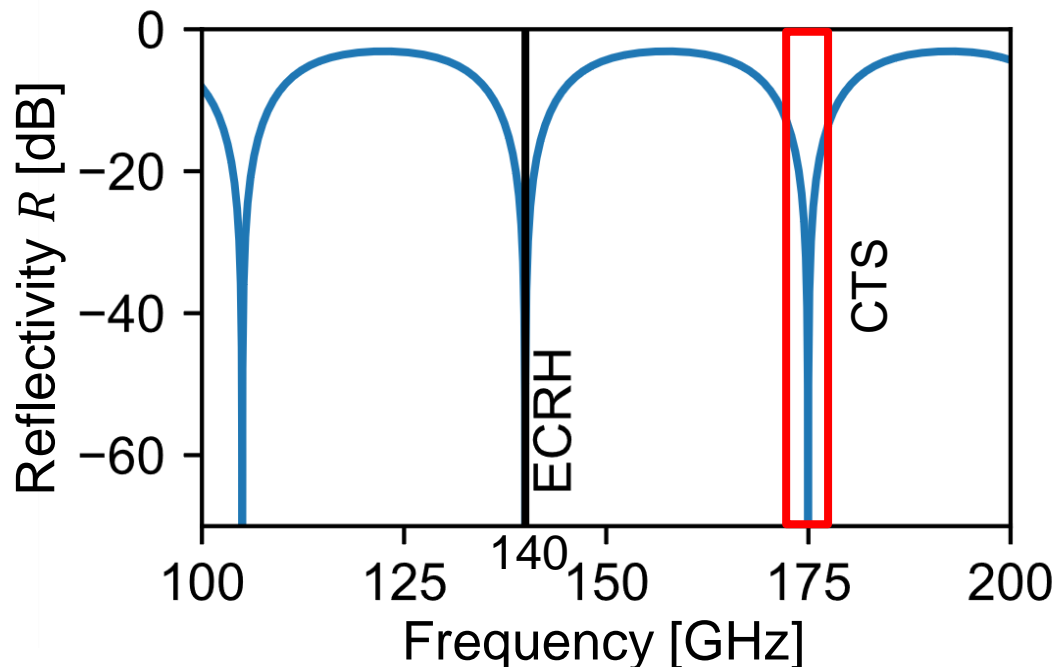
# Window Transmission

- Diamond window is transparent if window thickness  $d_w$  is a multiple of half of the wavelength inside the window:

$$d_w = m \frac{\lambda}{2} \quad \Leftrightarrow \quad f = m \frac{c_0}{2\sqrt{\epsilon_r}d_w} \quad \text{with } m = 1, 2, \dots; d_w = 1.8 \text{ mm};$$

$$\epsilon_r = 5.67$$

- Closest higher frequency compatible with the window thickness: **175 GHz**



| $m$ | $f$ [GHz] |
|-----|-----------|
| 3   | 105       |
| 4   | 140       |
| 5   | 175       |

Frequency range for  $R < 2.5 \%$ :  
173.2 GHz - 176.8 GHz

# Identification of Possible TE Modes

- Nominal mode for operation at 140 GHz:  $TE_{28,8}$ 
  - ➔ Operation at 175 GHz requires different TE mode

- Criteria for a suitable TE mode:

**Cut-off frequency  $f_c$ :** Excitation of the mode near cut-off frequency

➔ Should be close to 175 GHz for low reflections at the window

**Caustic radius  $r_c$ :** Determines conversion into Gaussian beam

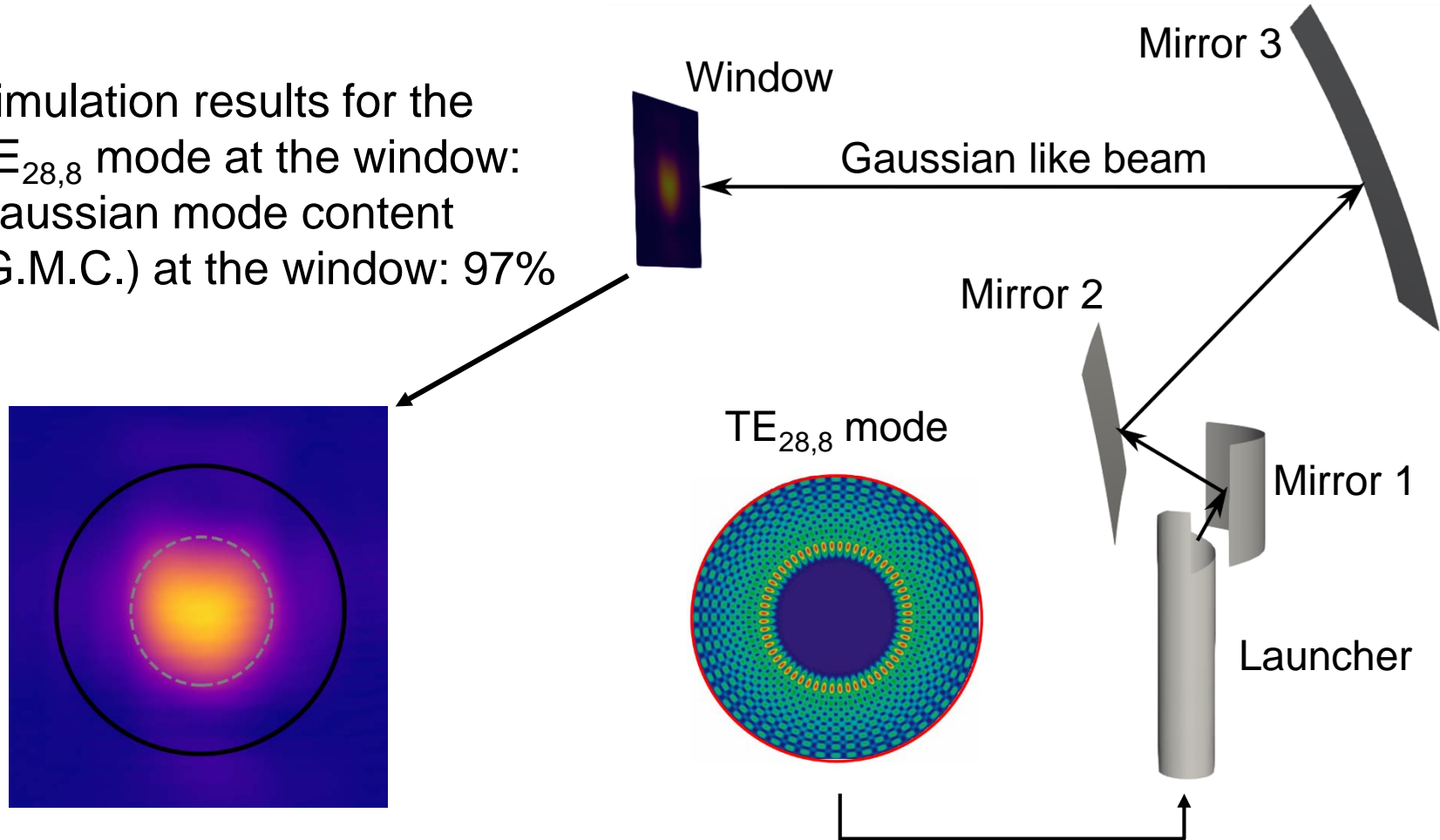
➔ Should be close to the one of the nominal  $TE_{28,8}$

| Mode         | $f_c$ [GHz] | $R$ [%] | $r_c$ [mm] |
|--------------|-------------|---------|------------|
| $TE_{28,8}$  | 140.02      | 0.002   | 10.2       |
| $TE_{29,12}$ | 175.26      | 0.07    | 8.44       |
| $TE_{32,11}$ | 176.08      | 0.96    | 9.27       |
| $TE_{34,10}$ | 173.72      | 1.18    | 9.99       |
| $TE_{35,10}$ | 176.59      | 2.00    | 10.11      |

# Launcher and Mirror System

- Launcher converts the cylindrical TE mode into a Gaussian like beam

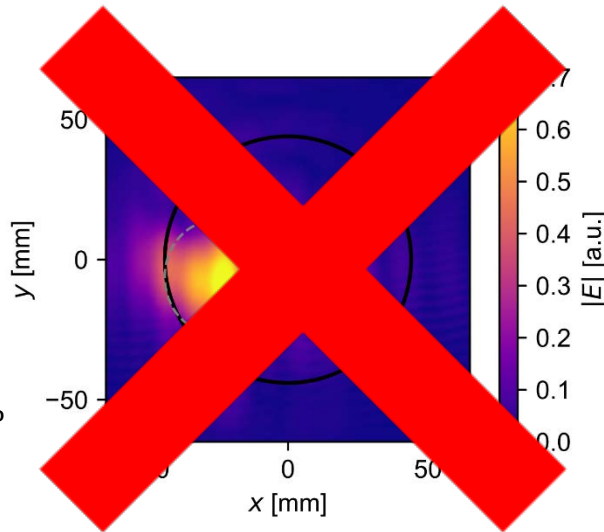
- Simulation results for the  $TE_{28,8}$  mode at the window:  
Gaussian mode content (G.M.C.) at the window: 97%



# Candidate Modes at the Window

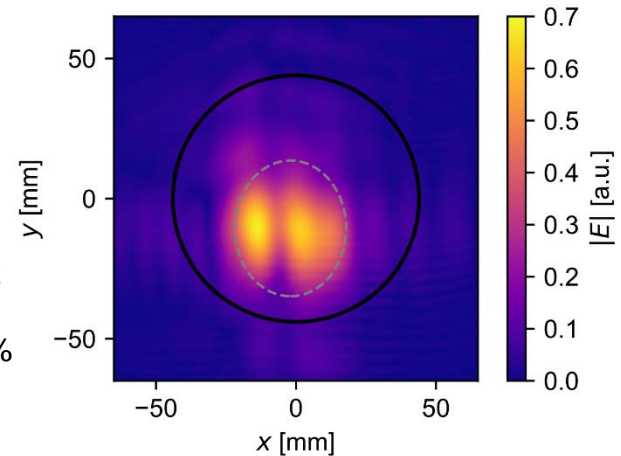
**TE<sub>29,12</sub>**

$f_c = 175.2$  GHz  
 $r_c = 8.44$  mm  
G.M.C. = 70.9%  
 $R = 0.07\%$



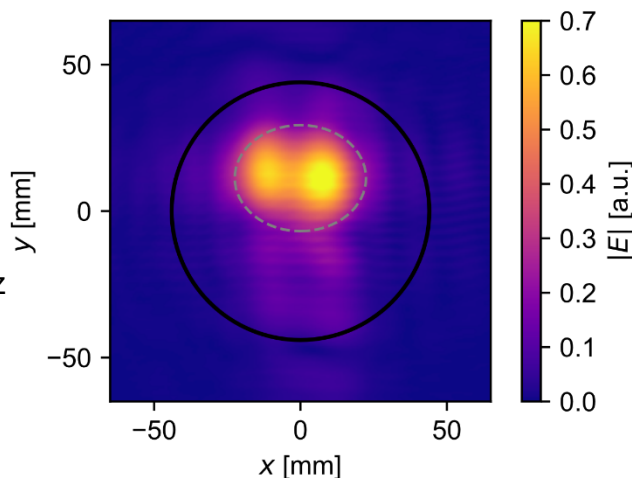
**TE<sub>32,11</sub>**

$f_c = 176.1$  GHz  
 $r_c = 9.27$  mm  
G.M.C. = 76.3%  
 $R = 0.96\%$



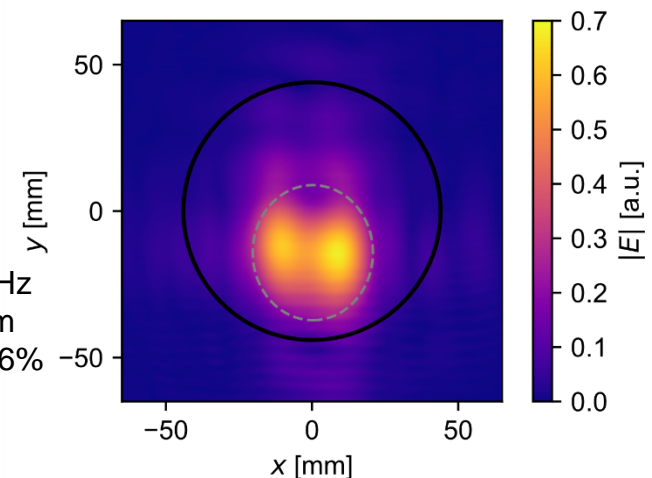
**TE<sub>34,10</sub>**

$f_c = 173.7$  GHz  
 $r_c = 9.99$  mm  
G.M.C. = 87%  
 $R = 1.18\%$



**TE<sub>35,10</sub>**

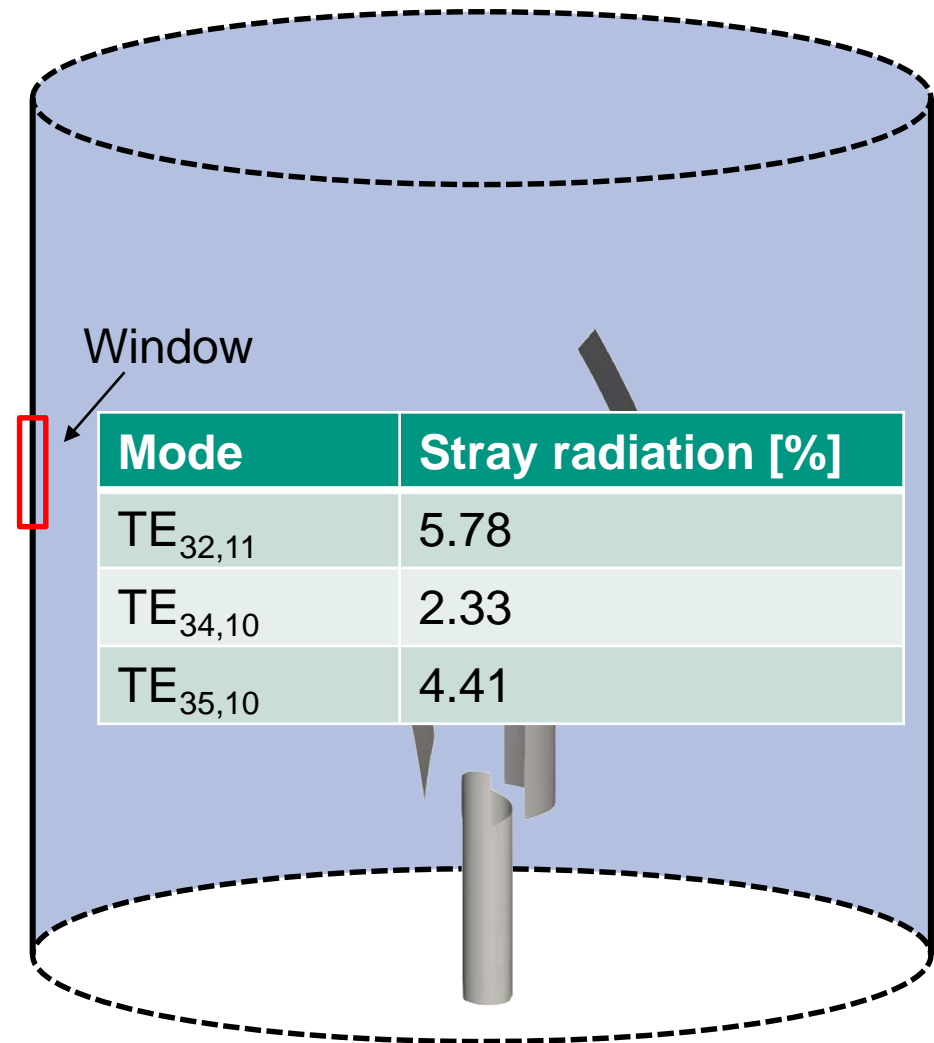
$f_c = 176.5$  GHz  
 $r_c = 10.11$  mm  
G.M.C. = 87.6%  
 $R = 2.00\%$



# Stray Radiation inside the Gyrotron

- Cylinder around the quasi-optical system
  - Radius: 300 mm
  - Length: 1200 mm
- Calculation of total power on the cylinder surface  $P_{\text{tot}}$
- Calculation of power exiting the window  $P_{\text{window}}$
- Stray radiation:

$$\frac{P_{\text{tot}} - P_{\text{window}}}{P_{\text{tot}}}$$



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# Electron Gun Operation

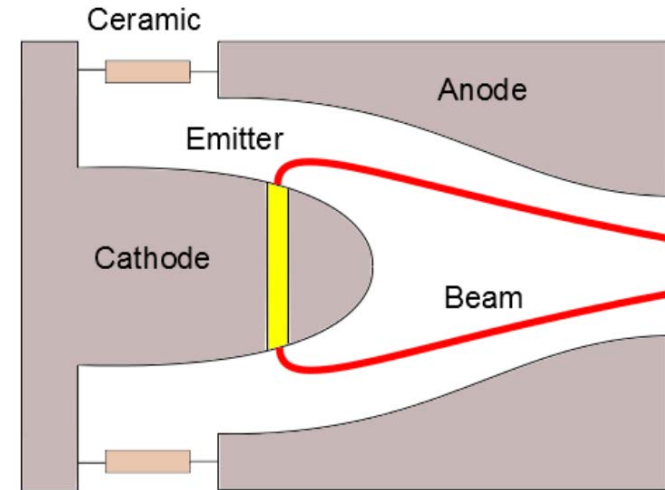
- Geometry of W7-X electron gun is fixed
- Parameters which can be changed:

**Beam voltage  $V_b$**

**Beam current  $I_b$**

**Magnetic field  $B_c$**

- Definition of operating points (OPs)
  - ➔ calculation of  $V_b$  and  $I_b$  depending on  $B_c$  based on simplified calculations to get an output power of 500 kW



| OP  | $B_c$<br>[T] | $V_b$<br>[kV] | $I_b$<br>[A] |
|-----|--------------|---------------|--------------|
| OP1 | 6.6          | 45            | 53           |
| OP2 | 6.7          | 54            | 45           |
| OP3 | 6.8          | 62            | 39           |
| OP4 | 6.9          | 71            | 34           |
| OP5 | 7.0          | 79            | 31           |



# Electron Beam Parameters

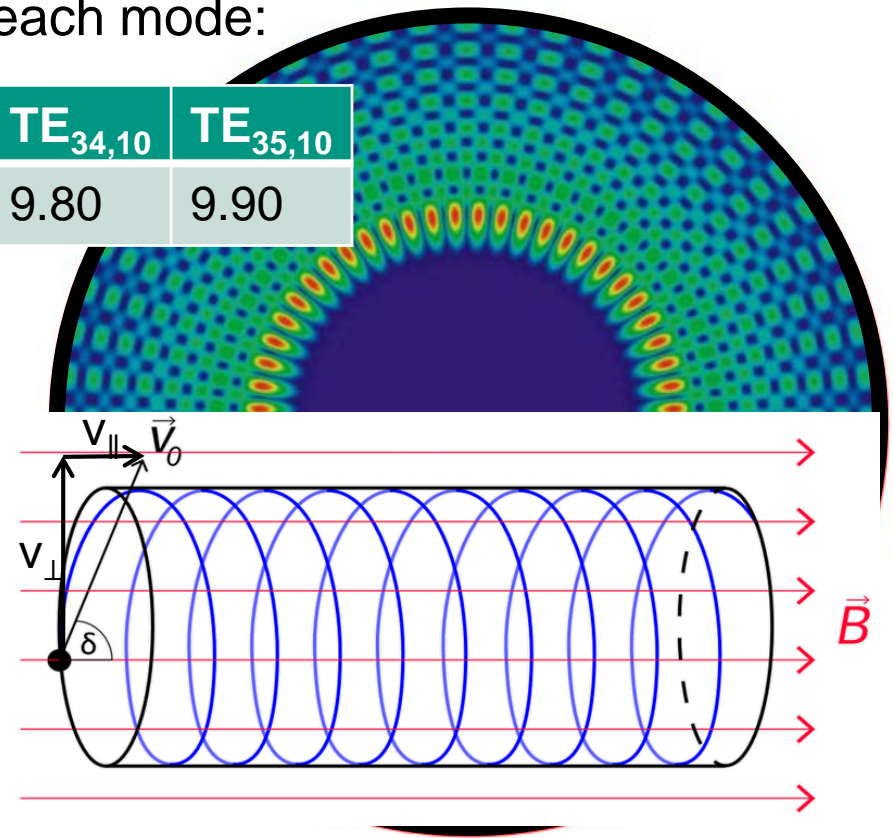
- Electron gun forms a hollow cylindrical electron beam

- Optimal guiding center radius for each mode:

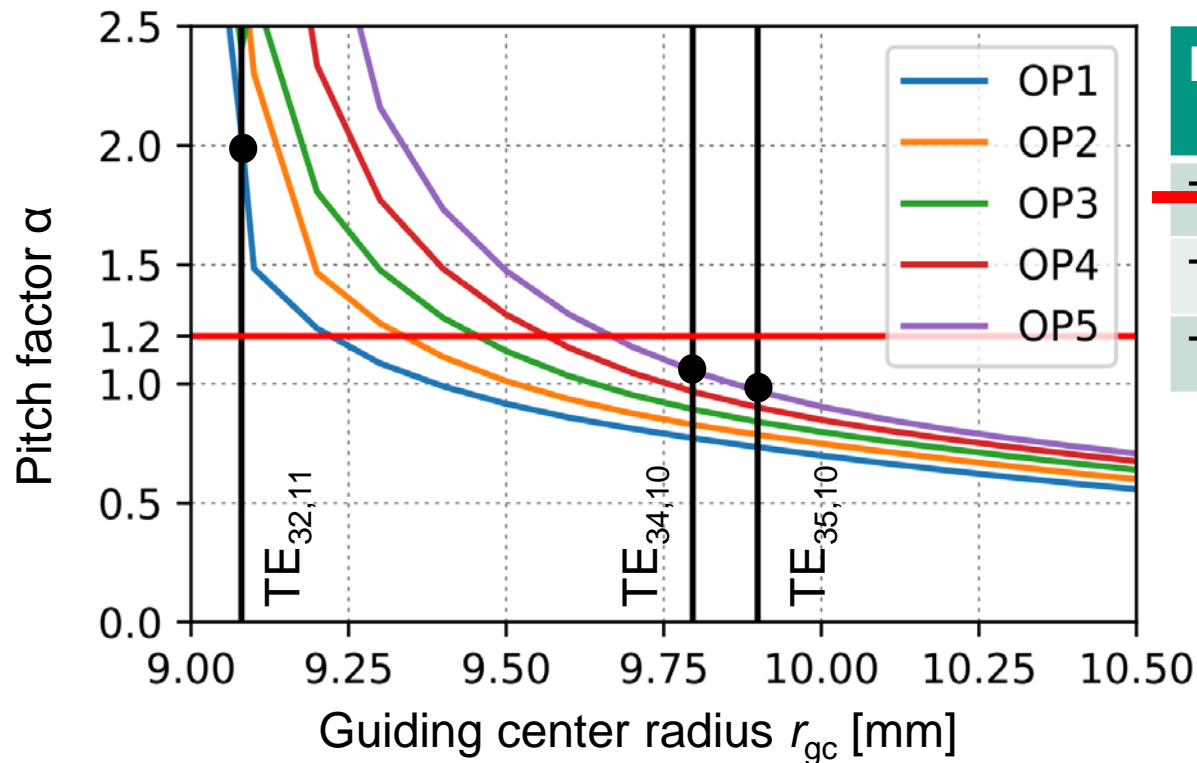
TE<sub>28,8</sub> mode

| mode                  | TE <sub>28,8</sub> | TE <sub>32,11</sub> | TE <sub>34,10</sub> | TE <sub>35,10</sub> |
|-----------------------|--------------------|---------------------|---------------------|---------------------|
| optimal $r_{gc}$ [mm] | 10.00              | 9.08                | 9.80                | 9.90                |

- Pitch factor  $\alpha = \frac{r_{gc} v_{\perp}}{v_{\parallel} B}$ 
  - Low pitch factor: no excitation of the mode in the cavity
  - High pitch factor: reflected electrons
  - Typical values: 1.2 – 1.4



# Simulation of the Electron Gun



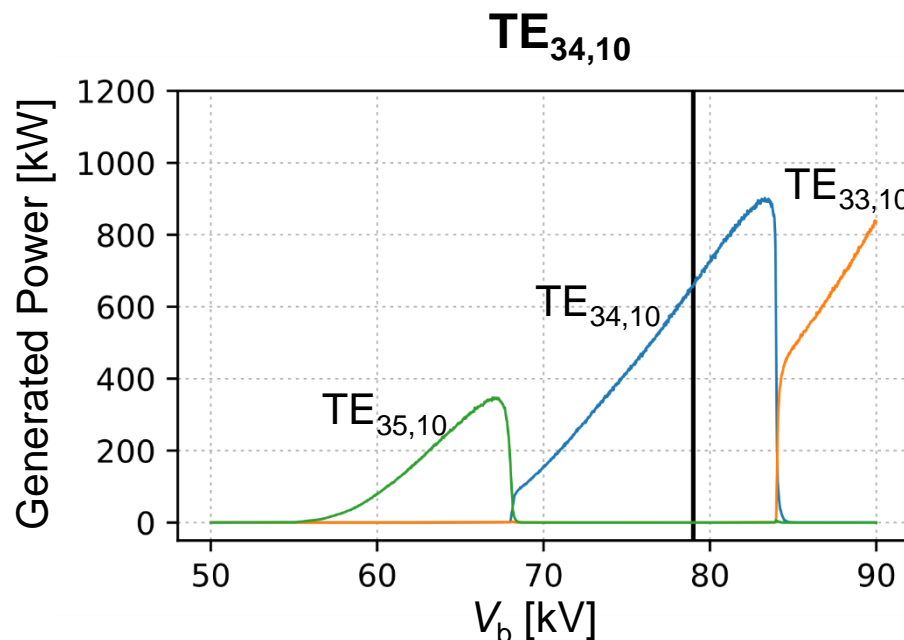
| Mode                               | Operating Point | $\alpha$        |
|------------------------------------|-----------------|-----------------|
| <del><math>TE_{32,11}</math></del> | <del>OP1</del>  | <del>2.00</del> |
| $TE_{34,10}$                       | OP5             | 1.05            |
| $TE_{35,10}$                       | OP5             | 0.97            |

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# Excitation in the Cavity (1/2)

- Multi-mode analysis for mode competition
  - Competitor modes could disturb excitation of desired mode
  - 40 potential competitor modes were analyzed
  
- Generated power in dependence of beam voltage:



Operating Parameters:

$$B_c = 6.98 \text{ T}$$

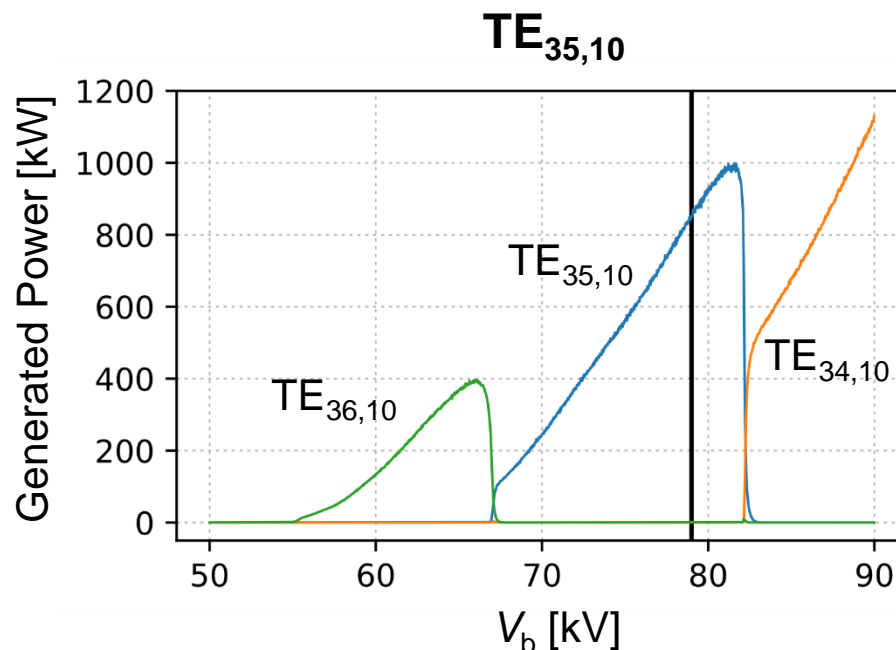
$$I_b = 40 \text{ A}$$

$$V_b = 79 \text{ kV}$$

Generated Power at  
nominal  $V_b$ : 660 kW

## Excitation in the Cavity (2/2)

- Multi-mode analysis for mode competition
  - Competitor modes could disturb excitation of desired mode
  - 40 potential competitor modes were analyzed
  
- Generated power in dependence of beam voltage:



Operating Parameters:

$$B_c = 7.10 \text{ T}$$

$$I_b = 50 \text{ A}$$

$$V_b = 79 \text{ kV}$$

Generated Power at  
nominal  $V_b$ : 850 kW

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# Conclusion

- Simulations show that it is possible to operate the W7-X gyrotron at 175 GHz for CTS

| Mode                             | TE <sub>34,10</sub> | TE <sub>35,10</sub> |
|----------------------------------|---------------------|---------------------|
| Excited frequency [GHz]          | 173.9               | 176.7               |
| <b>Window reflection [%]</b>     | <b>0.8</b>          | <b>2.5</b>          |
| <b>Stray radiation [%]</b>       | <b>2.33</b>         | <b>4.41</b>         |
| Gaussian mode content [%]        | 87.0                | 87.6                |
| Output power [kW]                | 660                 | 850                 |
| Efficiency [%]                   | 22                  | 22                  |
| Beam voltage [kV]                | 79                  | 79                  |
| Beam current [A]                 | 40                  | 50                  |
| Magnetic field at the cavity [T] | 6.98                | 7.10                |

# Outlook

- Procurement of a new magnet
  - Operation at 175 GHz requires 7 T at the cavity
  - Current magnet used for the 140 GHz operation can not deliver 7 T
  
- New Magnet should allow operation at 140 GHz and 175 GHz
  - Discussions with different magnet suppliers are ongoing
  - Magnetic profile for the 140 GHz operation of the new magnet needs to be identical to the magnetic profile of the old magnet
  - In previous simulations, for the 175 GHz operation, the magnetic profile of the 140 GHz operation (upscaled to 7 T) was used
  - Difficulties for the magnet suppliers to deliver a magnet with the requested profiles for the 140 GHz and 175 GHz operation → variations in the magnetic profile for the 175 GHz operation
  
- ➔ New simulations for the 175 GHz operation with the magnetic profile provided by the magnet suppliers



# Thank you very much for your attention