

USING FOWLER-NORDHEIM PLOT FOR THE COMPARISON OF ELECTRON EMISSION EFFICIENCY OF FIELD (FE) AND THERMAL EMISSION (TE) CATHODES

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**7th ITG International Vacuum Electronics Workshop (IVEW) 2020
and
13th International Vacuum Electron Sources Conference (IVeSC) 2020**

planned for Physikzentrum Bad Honnef (PBH), Bad Honnef, Germany
(virtual conference/Thales AVS France, Paris),

May 26-29, 2020,

Lecture IVEW23, May 26, 2020, 15:30 CEST (3:30 p.m.)

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OUTLINE:

1. Introduction

2. Motivation

3. Definition of Electron Emission Efficiency (3E)

4. Fowler Nordheim (FN) plot

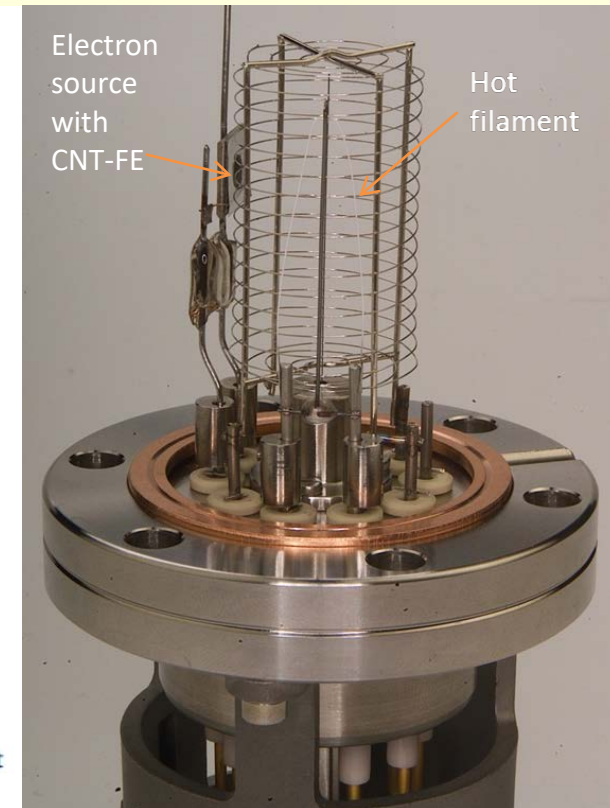
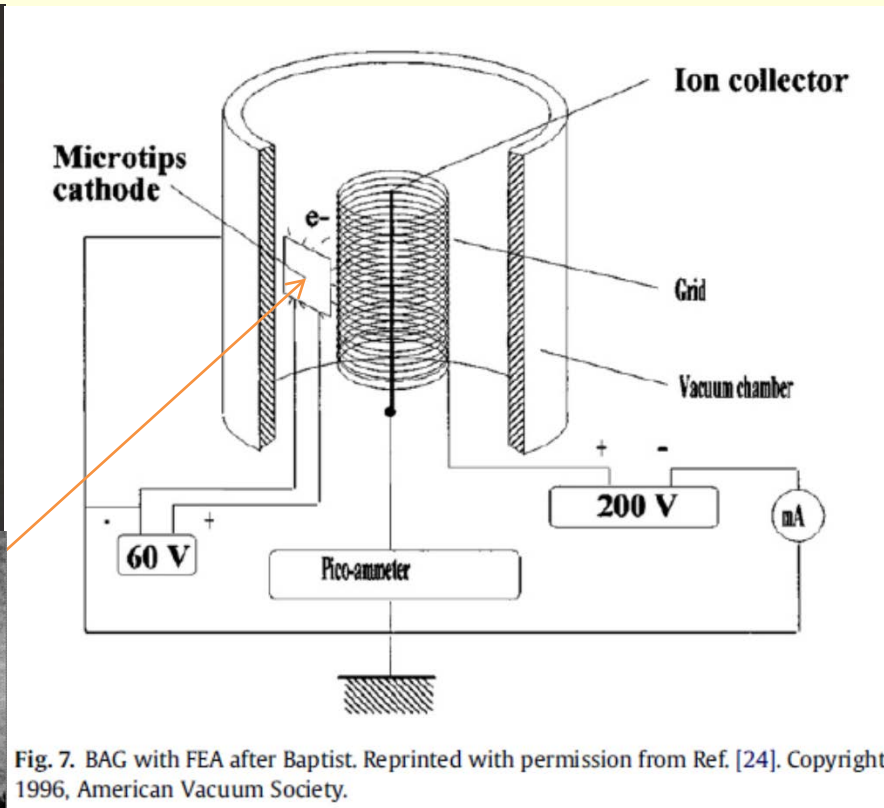
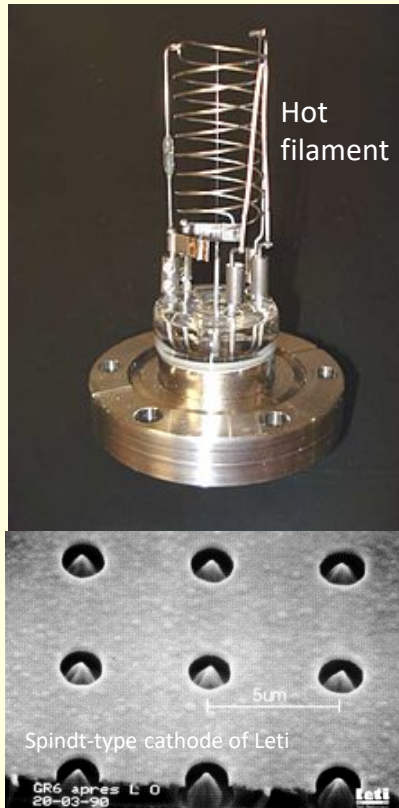
- Standard use of the FN plot for field emission analysis
- Extended use of the FN plot for comparison of electron emission efficiency

5. Comparison of field (FE) and thermal (TE) cathodes

6. Conclusion and outlook

Motivation: Ionization Gauges

Typical application of cathodes with **1 mA** emission current and the question:
What is better?



Ionization gauge with thermal (hot filament) or field emitter cathodes (Spindt-type [1], CNT-FE [2], SS [3])

Literature:

- [1] R. Baptist, C. Bieth, C. Py: Bayard–Alpert vacuum gauge with microtips, J. Vac. Sci. Techn. B, 14 (1996) 2119-2125.
- [2] W. Knapp, D. Schleussner, M. Wüest: Investigation of ionization gauges with carbon nanotube (CNT) field-emitter cathodes. J. of Physics: Conf. Series 100 (2008) 092007.
- [3] W. Knapp, M. Wüest: “Vacuum measuring gauge”, patent WO 2006/094687, priority data 04.03.2005.

Knapp, Wolfram: „Using Fowler-Nordheim plot for the comparison of electron emission efficiency of field (FE) and thermal emission (TE) cathodes. 7th ITG International Vacuum Electronics Workshop (IVEW) 2020 and 13th International Vacuum Electron Sources Conference (IVESC) 2020 , planned for Physikzentrum Bad Honnef (PBH), Germany (virtual conference/Thales AVS France), May 26-29, 2020, Lecture IVEW23, May 26, 2020, 3:30 pm MESZ.

Electron Emission Efficiency - Definition

Electron Emission Efficiency (3E):

$$\nu_{3E} = \frac{\text{emission current } I_E}{\text{spent electrical power } P_{el}} = \frac{I_E}{P_{el}} \quad [V^{-1}]$$

The relation I_E/P_{el} , easy to measure (e.g. for TE is $P_{el} = P_{heat}$), is therefore a simple criterion reflecting the electron emission efficiency, independent of the kind of electron emission mechanism (Tab. 1):

Table 1. Comparison of the electrical power P_{el} for different typical cathode types (without significant loss of power)

Cathode:	Cold Field Emitter FE	Thermionic TE (Hot Filament)	Dispenser-C. (with Schottky effect)	Plasma-C. or Electron Source
$P_{el} =$	$P_{extr} = I_E \cdot U_{extr}$	$P_{heat} = I_{heat} \cdot U_{heat}$ ($= I_f \cdot U_f$)	$P_{heat} (+ P_{extr})$ cf. TE- (and FE-) Cathodes	$P_{pl} = I_{pl} \cdot U_{pl}$ [$+ P_{extr}$]



A special case is the emission efficiency of FE cathodes:

$$\nu_{3E_FE} = \frac{I_E}{P_{extr}} = \frac{1}{U_{extr}} \quad [V^{-1}].$$

That means that $\frac{1}{U_{extr}}$ (and so U_{extr} !) is a directly measure of the emission efficiency of FE cathodes.

But also the inverse extraction voltage $\frac{1}{U_{extr}} [V^{-1}]$ is the **abscissa of the Fowler-Nordheim (FN) plot!**

The comparison with other emission mechanism is based on the calculation of a fictive extraction

voltage: $U_{extr}^* = P_{el}/I_E$ The resulting **FN plot ordinate** is $\ln(I_E/(U_{extr}^*)^2)$ for all electron emissions.

Fowler Nordheim (FN) plot

Standard use: measurement and calculation of field enhancement factor β

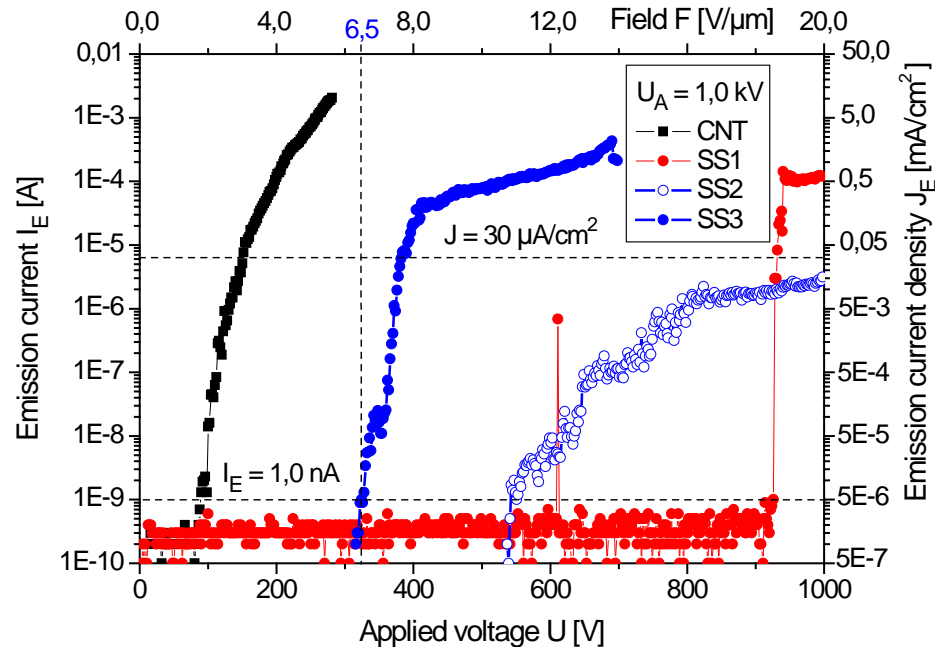


Fig. 1 Field-emission (FE) characterization of three stainless steel samples SS1, SS2 and SS3, and CNT Buckypaper with the same area for comparing [1]. For sample SS3 the current density value $J = 30 \mu\text{A}/\text{cm}^2$ lies significantly below the saturation characteristic.

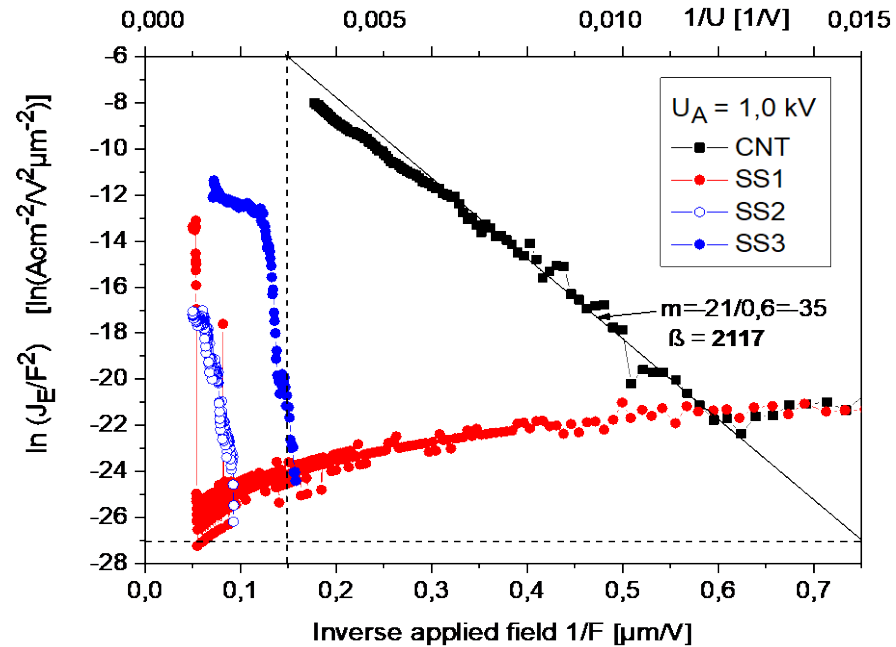


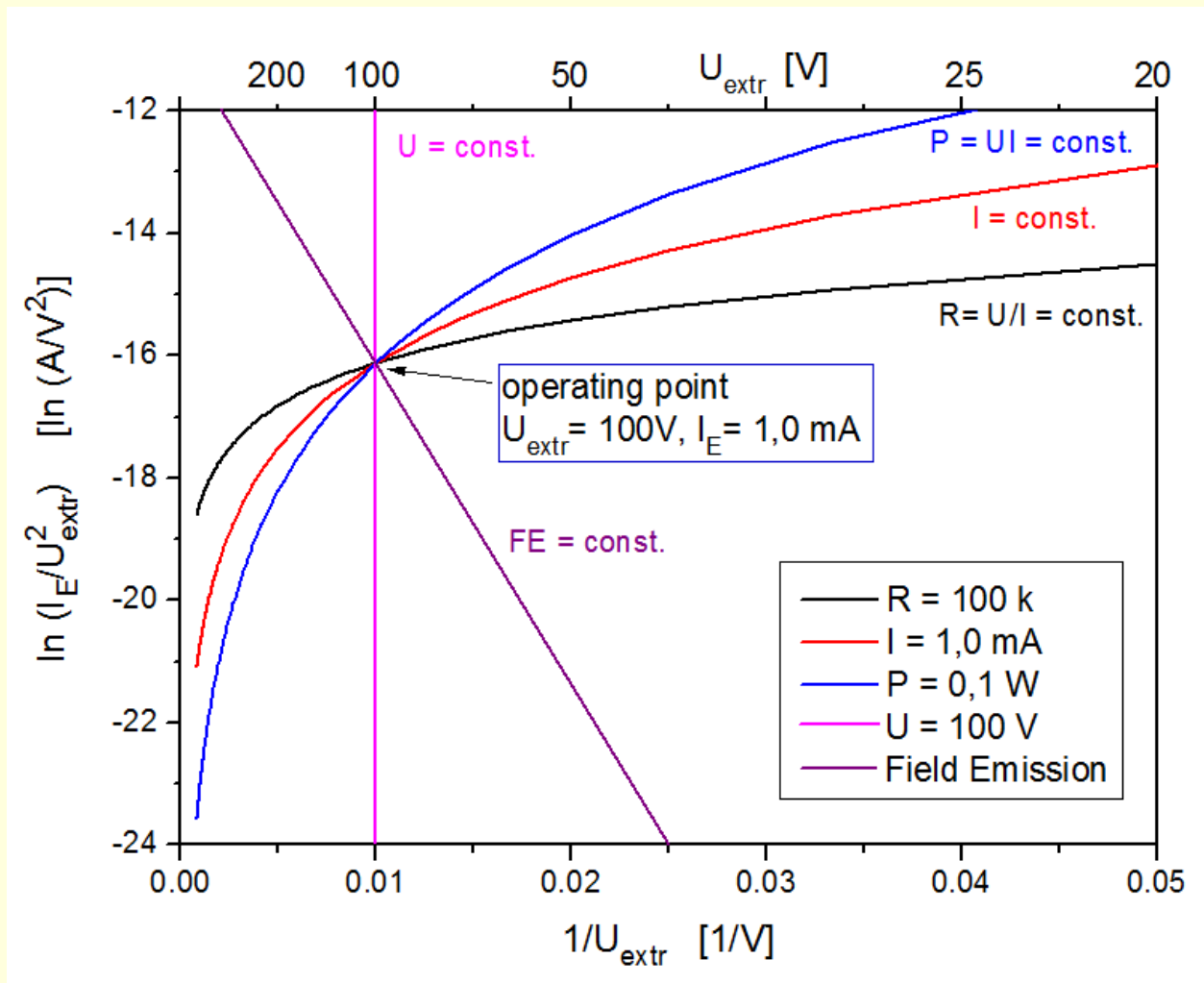
Fig. 2 Fowler-Nordheim plot (FN plot) of FE measurements in Fig. 1. and with graphic presentation of slope m for β_{CNT} calculation [2]:

$$\beta_{CNT} = - (B \cdot \Phi^{3/2}) / m$$

[1] W. Knapp, D. Schleussner, "Field-emission characteristics of carbon buckypaper", JVST B 21 557-561 (2003).

[2] W. Knapp "Field-emission investigations of micro-structured stainless steel 1.4301 (ASTM 304) for extended use of vacuum components as very large FE cathode arrays." Poster, IVNC 2017.

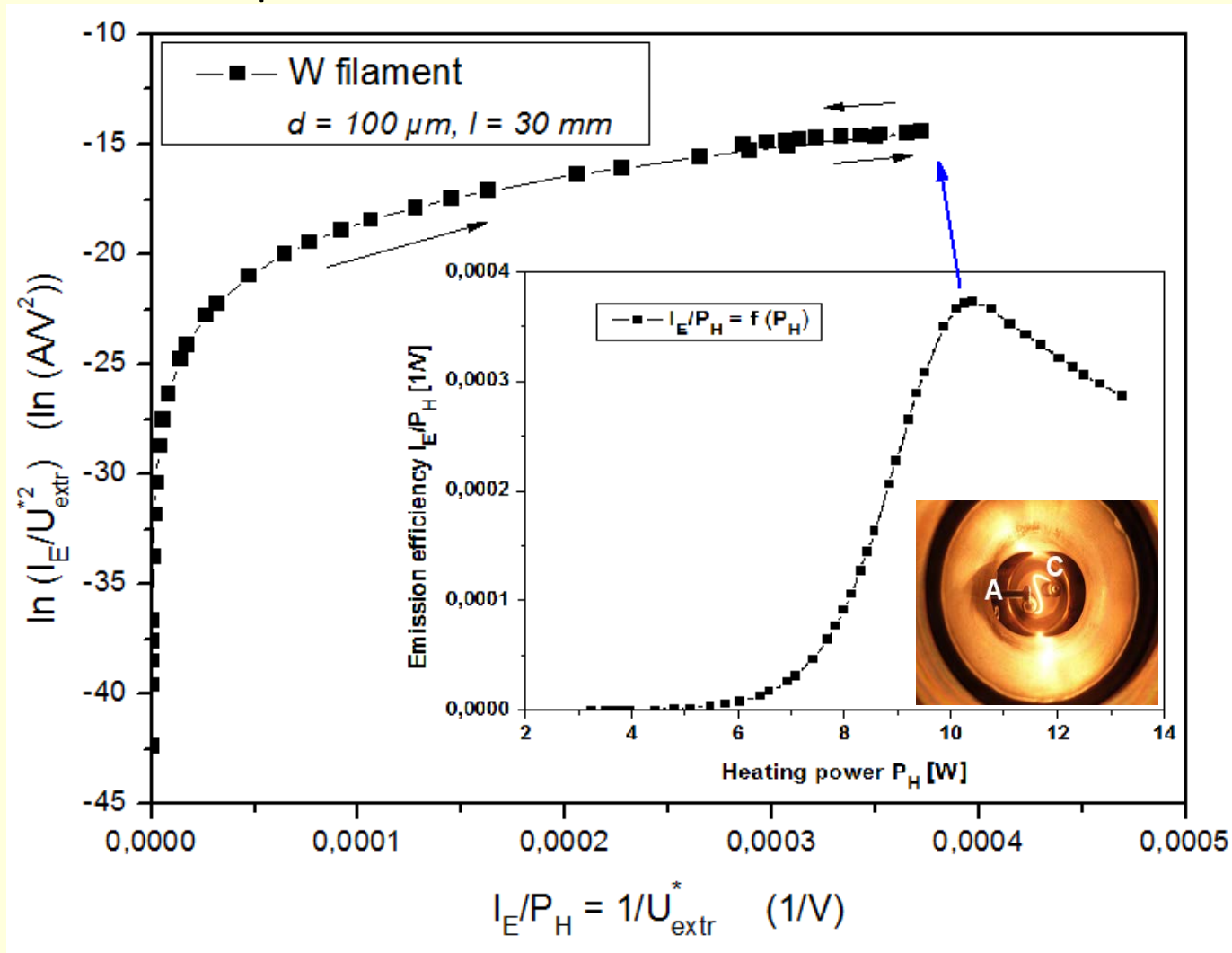
Fowler Nordheim (FN) plot



FN plot with constant characteristics based on an operating point

Fowler Nordheim (FN) plot

1st FN plot with hot filament characteristic



FN plot of HF cathode with increasing emission efficiency, cf. inside $I_E/P_{\text{Heat}} = f(P_{\text{Heat}})$

Comparison of field (FE) and thermal (TE) cathodes

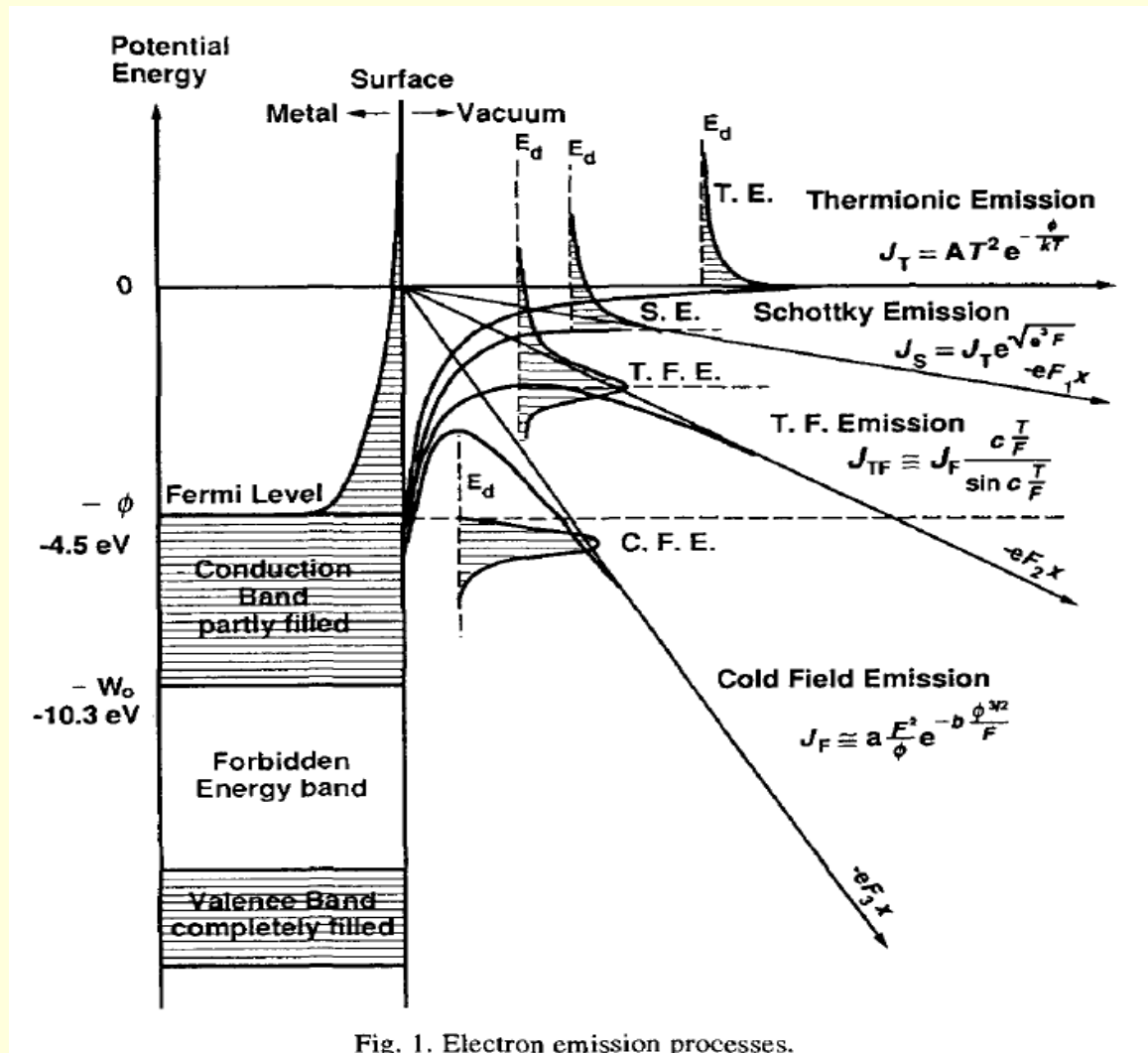
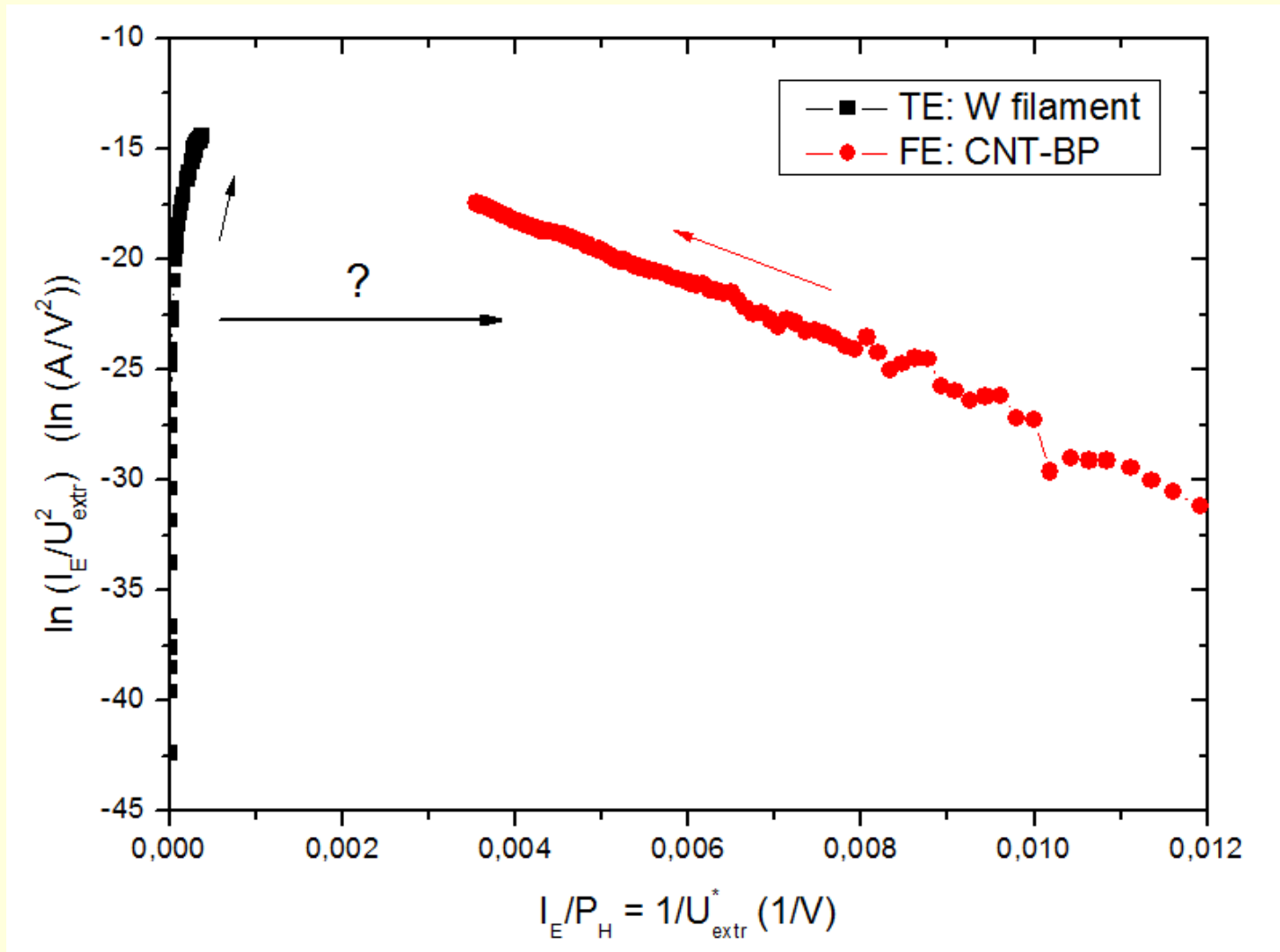


Fig. 1. Electron emission processes.

Lit.: F. Charbonnier: Developing and using the field emitter as a high intensity electron source, Applied Surface Science 94/95 (1996), p. 26-43.

Comparison of field (FE) and thermal (TE) cathodes



FN plot comparison of field (CNT-FE) and thermal TE cathodes (HF of BAG)

Comparison of field (FE) and thermal (TE) cathodes

Vacuum tubes with indirectly heated cathodes

Elektronenröhre ECC83, Doppeltriode

9-pol

Elektronenröhre ist ein weltweit renommierter Hersteller von Vakuumröhren. Elko's und High-Audioverstärker. Die Röhren werden häufig in Gitarren- und Audioverstärkern und vielen anderen Anwendungsbereichen im Bereich Audio eingesetzt.

Anodenspannung: 250 V
Anodenstrom: 1,2 mA
Heizungsspannung: 6,3 / 12,6 V
Heizungsstrom: 300 / 150 mA
Maße: Ø 22,0 x 55,3 mm

Bestell-Nr.: TUBE ECC83JJ

19% SPAREN **9,90**

Elektronenröhre EL12N, Leistungs- röhre

Y8A, 8-pol

Anodenspannung: 250 V
Anodenstrom: 72 mA
Heizungsspannung: 6,3 V
Heizungsstrom: 1,2 A
Maße: Ø 38 x 95 mm

Bestell-Nr.: TUBE EL12N X2 23,30
TUBE EL12N X4 46,60

Anzahl: einzeln, matched Pair, matched Quartett

Elektronenröhre PC900, Triode

7-pol, für Fassung: B7G

Anodenspannung: 135 V
Anodenstrom: 20 mA
Heizungsspannung: 3,9 V
Heizungsstrom: 300 mA
Maße: Ø 19 x 41,2 mm

Bestell-Nr.: TUBE PC900 1,80

Elektronenröhre EL84, Endstufenröhre

9-pol

Anodenspannung: 250 V
Anodenstrom: 49 mA
Heizungsspannung: 6,3 V
Heizungsstrom: 760 mA
Maße: Ø 22 x 77,8 mm

Bestell-Nr.: TUBE EL84 X2 30,95
TUBE EL84 X4 62,60

Anzahl: einzeln, matched Pair, matched Quartett

Elektronenröhre PCF86, Mehrfachröhre

Noval, 9-pol

Anodenspannung: 170 V
Anodenstrom: 14 mA
Heizungsspannung: 8 V
Heizungsstrom: 300 mA
Maße: Ø 22,2 x 55,6 mm

Bestell-Nr.: TUBE PCF86 1,80

Elektronenröhre ECC82, Doppeltriode

Noval, 9-pol

Anodenspannung: 250 V
Anodenstrom: 10,5 mA
Heizungsspannung: 6,3 / 12,6 V
Heizungsstrom: 300 / 150 mA
Maße: Ø 19 x 41,2 mm

Bestell-Nr.: TUBE ECC82JJ 11,20

Elektronenröhre C3C, Pentode

8-pol, für Fassung: Y8A

Anodenspannung: 220 V
Anodenstrom: 10 mA
Heizungsspannung: 4 V
Heizungsstrom: 1,1 A
Maße: Ø 53 x 148 mm

Bestell-Nr.: TUBE C3C 4,45

Elektronenröhre EDD11, Mehrfachröhre

Octal, für Fassung: Y8A

Anodenspannung: 250 V
Anodenstrom: 2x 17,5 mA
Heizungsspannung: 6,3 V
Heizungsstrom: 400 mA
Maße: Ø 36 x 57,5 mm

Bestell-Nr.: TUBE EDD11 5,35

Elektronenröhre EL 34B-STR, Endstufenröhre

Octal, 8-pol

Anodenspannung: 800 V
Kathodenstrom: 150 mA
Heizungsspannung: 6,3 V
Heizungsstrom: 1,5 A
Maße: Ø 36 x 114 mm

Bestell-Nr.: TUBE EL 34-S4A 37,30

Röhrenfassungen in verschiedenen Ausführungen

Typ B7G, 7-pol

Standard-Ausführung
Printmontage
Keramik

Bestell-Nr.: TUBE S B7G 0,99

Typ Y8A/Y10A, 8-/10-pol

Stahl-Ausführung
Lötmontage

Bestell-Nr.: TUBE S Y8A/Y10A 5,25

Draht-/Chassis, 9-pol

Draht-/Chassis
Lötmontage

Bestell-Nr.: TUBE S 9 DC 01 1,10

BESTELHOTLINE: +49 (0) 44 22 / 955 - 333

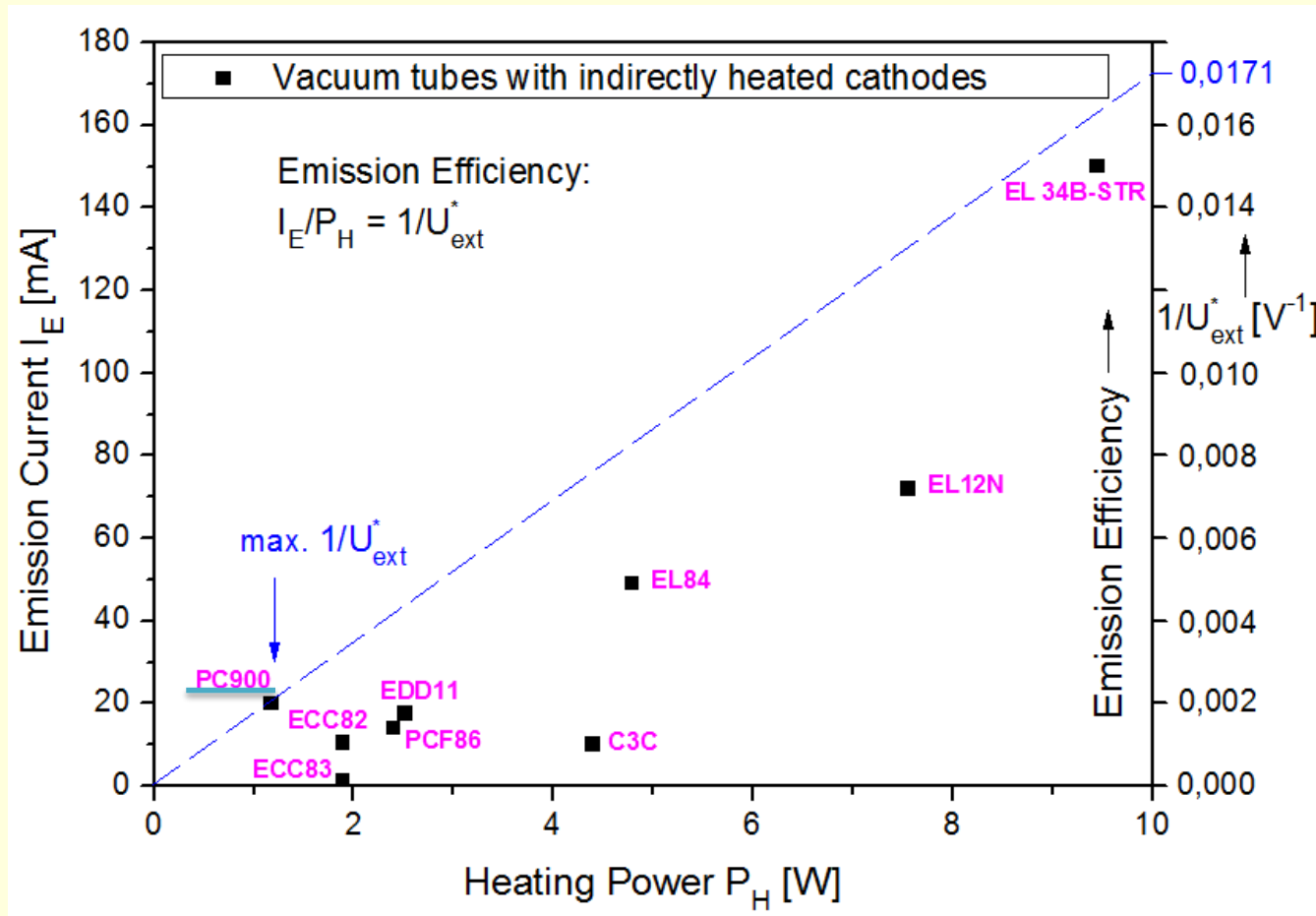
Tagespreise · Preisstand: 22.07.2019,
Preise in € inkl. MwSt., zzgl. Versandkosten

Gleich bestellen! www.reichelt.de

Lit.: [1] Amplifier tubes, catalogue BEST OF reichelt 8/2019, S.18/19 (or: www.reichelt.de)

Comparison of field (FE) and thermal (TE) cathodes

Vacuum tubes with indirectly heated cathodes

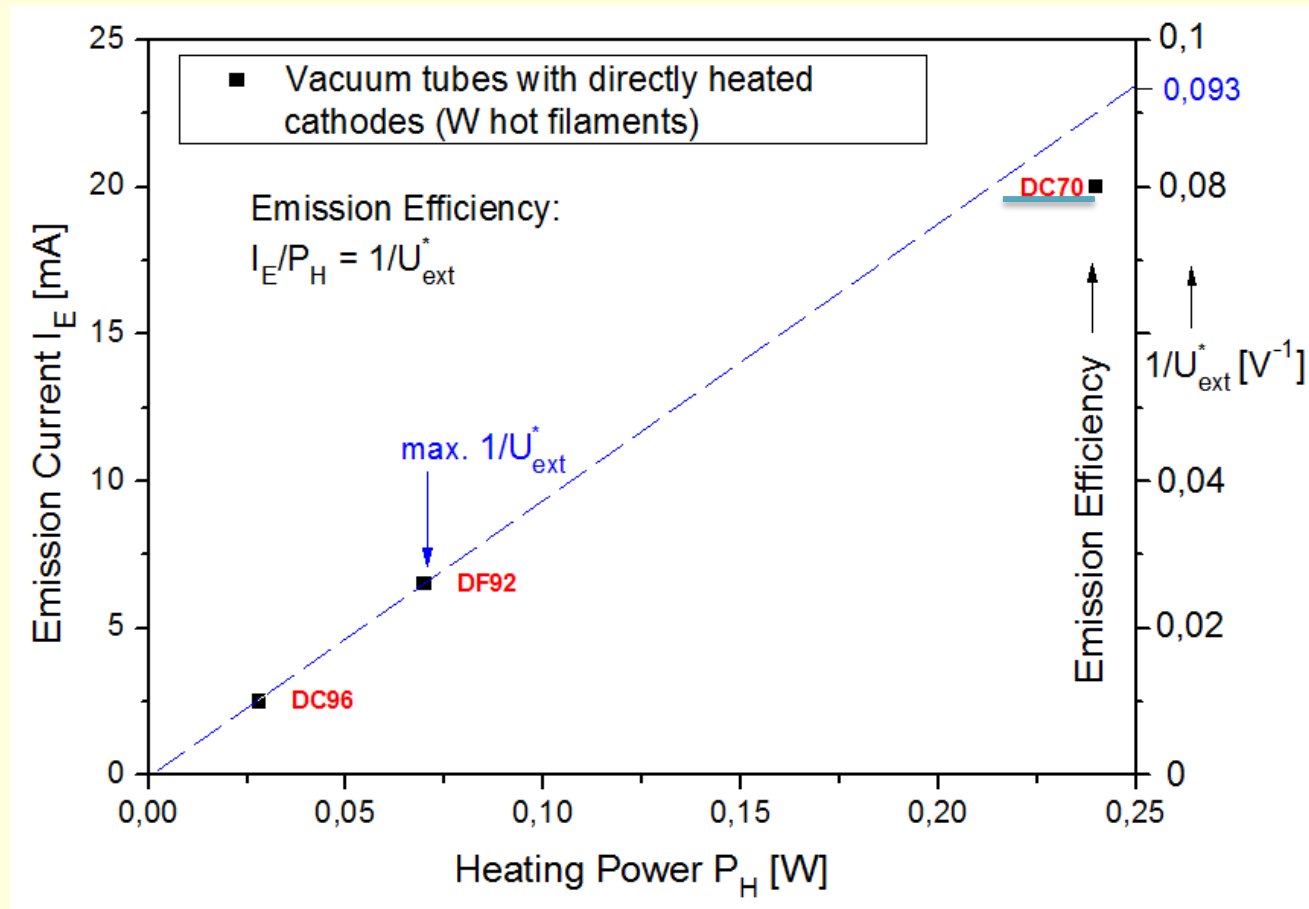


Selected vacuum tube: **PC900** (single hot filament, $I_H = 300$ mA, $I_E = 20$ mA) [1]

Lit.: [1] Amplifier tubes, catalogue BEST OF reichelt 8/2019, S.18/19 (or: www.reichelt.de)

Comparison of field (FE) and thermal (TE) cathodes

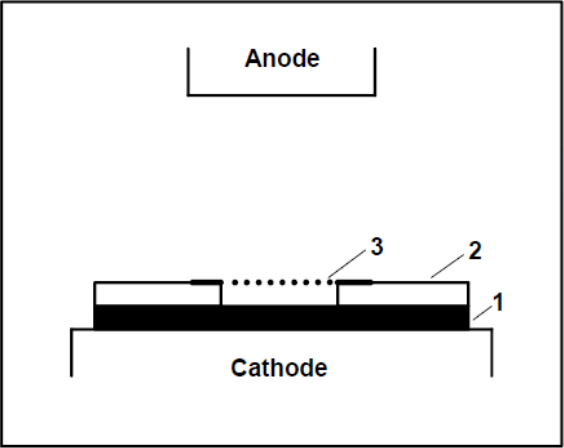
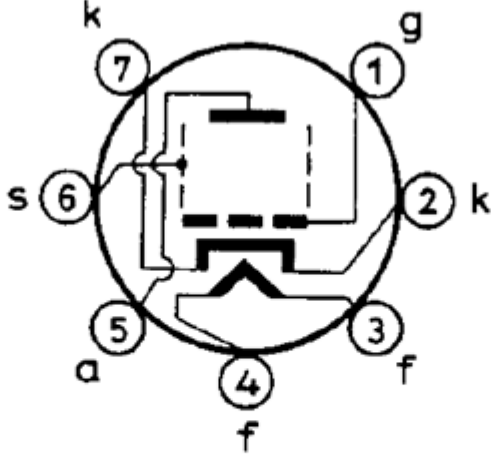
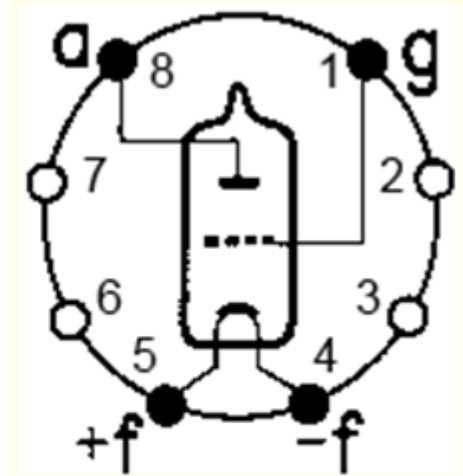
Vacuum tubes with directly heated cathodes



Selected vacuum tube: **DC70** (single hot filament, $I_H = 200$ mA, $I_E = 20$ mA)

Lit.: [1] Amplifier tubes, catalogue BEST OF reichelt 8/2019, S.18/19 (or: www.reichelt.de)

Comparison of field (FE) and thermal (TE) cathodes

Electron source with FE cathode [1]	<u>Cathode of triode PC900</u>	<u>Cathode of triode DC 70</u>
		
<p>Legend: 1 – cold field-emitter cathode with CNT <u>Buckypaper</u> 2 – spacer, 3 – micro grid</p>	<p>Legend: f – hot filament, k – cathode, indirectly heated g – grid, s – shield, a – anode</p>	<p>Legend: f – hot filament cathode, directly heated g – grid, a – anode</p>

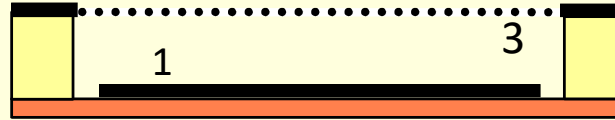
Schemes of triodes with compared FE and TE cathodes ($U_{\text{anode}} = 100 \text{ V}$)

Ref.: [1] W. Knapp, D. Schleußner: Special features of electron sources with CNT field emitter and micro grid. Applied Surface Science **251** (2005) 164–169.

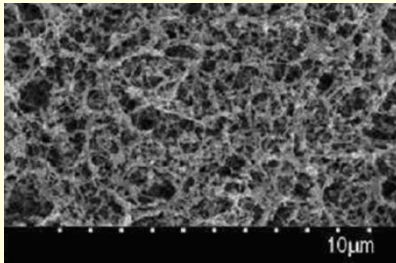
Comparison of field (FE) and thermal (TE) cathodes

Electron source with CNT field emission cathode for $I_E = 1$ mA (DC)
(reference source of Knapptron GmbH)

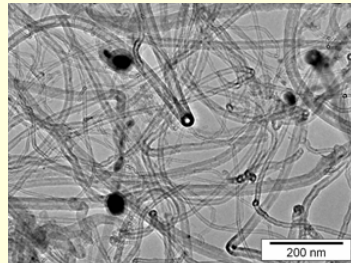
Layout of electron source :



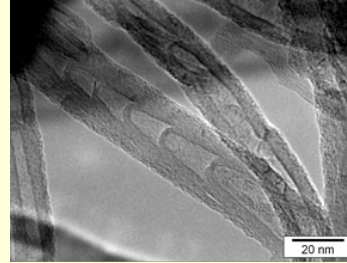
1. CNT field emission cathode with MWCNT [1]



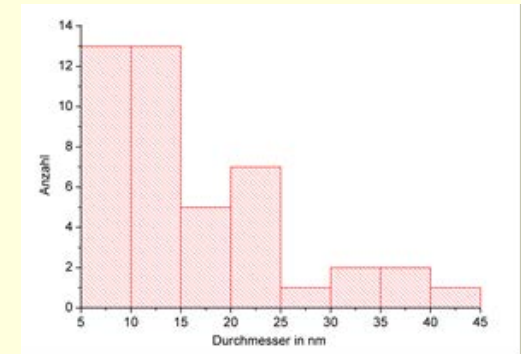
SEM image [10 μm]



TEM image 1 [200 nm]

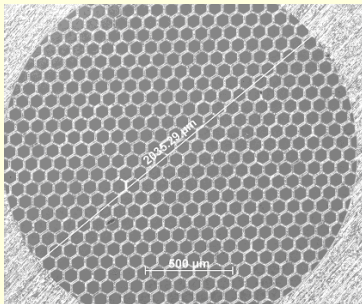


TEM image2 [20 nm]

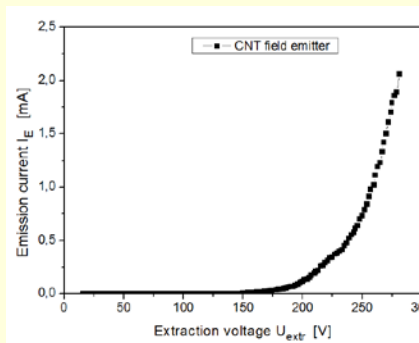
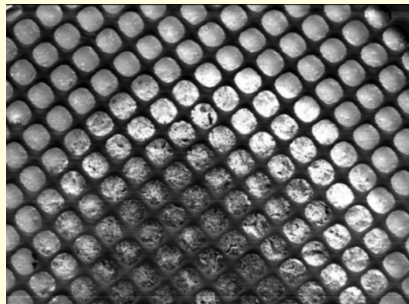


Distribution of d_{MWCNT} (TEM measurement)

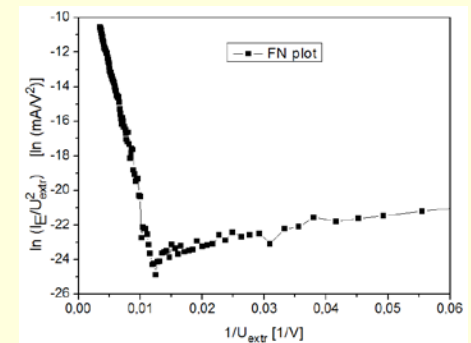
3. Micro grid [2]



Examples of micro grid



Electron field emission: $I = f(U)$ and



Fowler Nordheim (FN) plot

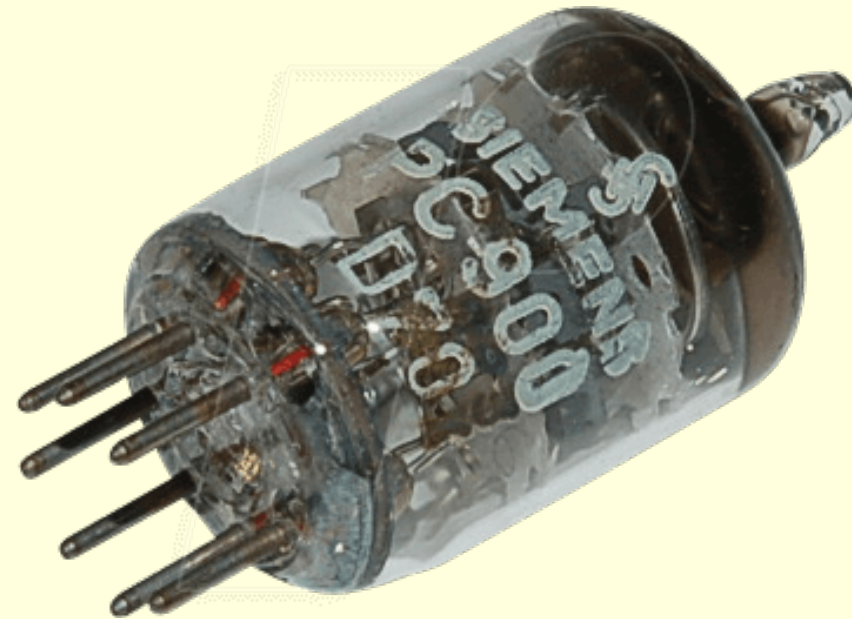
Lit.: [1] W. Knapp, D. Schleussner: Field-emission characteristics of carbon buckypaper. J. Vac. Sci. Technol. B 21 (2003) 1, 557 – 561.

[2] W. Knapp, D. Schleußner: Special features of electron sources with CNT field emitter and micro grid. Applied Surface Science 251 (2005) 164–169.

Comparison of field (FE) and thermal (TE) cathodes

Vacuum tube **PC900** (triode) with indirectly heated oxid cathode

		PC900
V.H.F. TRIODE		
Triode intended for use as R.F. amplifier in V.H.F. television receivers.		
QUICK REFERENCE DATA		
Cathode current	I_k max.	20 mA
Transconductance	S	20 mA/V
Amplification factor	μ	84
HEATING: Indirect by A.C. or D.C.; series supply		
Heater current	I_f	300 mA
Heater voltage	V_f	3.9 V



$$P_f = 1,17 \text{ W} \quad \text{and} \quad I_k = 20 \text{ mA}$$

$$\text{Emission efficiency: } I_k/P_f = 0,0171$$

$$\text{Fictive voltage: } U_{extr}^* = 58,5 \text{ V}$$

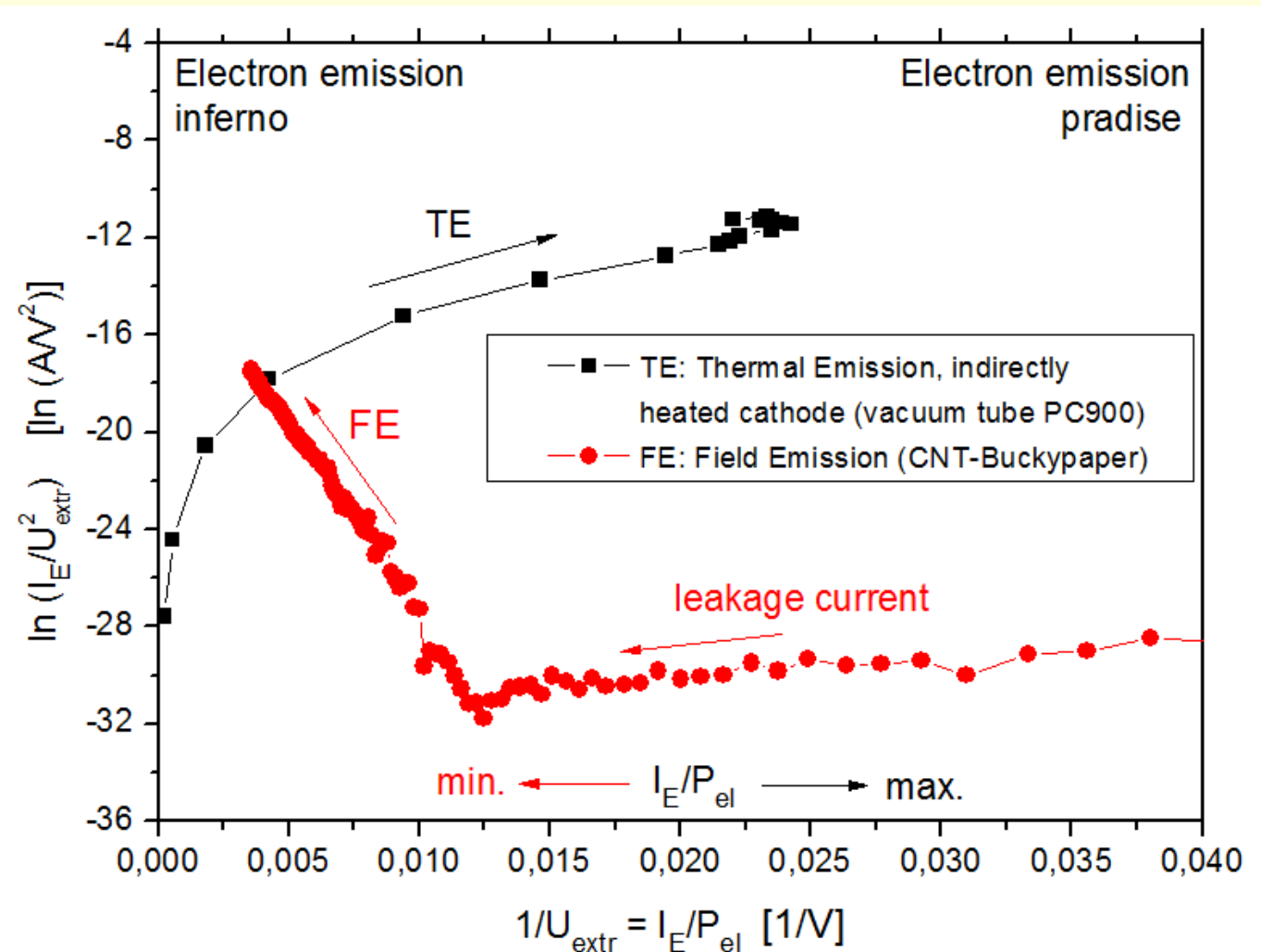
Actual price: 1,80 € (Germany)

$$P_f = 1,17 \text{ W}$$

Lit.: Data sheet PC900: https://cdn-reichelt.de/documents/datenblatt/A300/PC900_DB-EN.pdf (Januar 1970)

Knapp, Wolfram: „Using Fowler-Nordheim plot for the comparison of electron emission efficiency of field (FE) and thermal emission (TE) cathodes. 7th ITG International Vacuum Electronics Workshop (IVEW) 2020 and 13th International Vacuum Electron Sources Conference (IVESC) 2020 , planned for Physikzentrum Bad Honnef (PBH), Germany (virtual conference/Thales AVS France), May 26-29, 2020, Lecture IVEW23, May 26, 2020, 3:30 pm MESZ.

Comparison of field (FE) and thermal (TE) cathodes



FN plot comparison of field (CNT-FE) and thermal TE cathodes (indirectly heated)

Comparison of TE and FE Electron Emission Efficiency

Different trends in dependence on physical parameters T or U

→ TE: The emission in temperature-limited regime is described by the Richardson–Dushman equation:

$$J_0 = A_R T^2 e^{-\Phi/kT} \quad (1),$$

where J_0 [Acm⁻²] is the current density at zero-field, A_R [Acm⁻²K⁻²] is the Richardson constant, in the ideal case equal to the thermionic constant 120.4 [Acm⁻²K⁻²], Φ [eV] is the electronic work function, k [eV/K] is the Boltzmann constant and T [K] is the true cathode temperature. The emission efficiency is:

$$\nu_{E3_TE} = \frac{I_E}{P_{el}} \cong \frac{I_E}{P_{heat}} \cong \frac{A_C J_0}{Q(T)} = \frac{A_C [A_R T^2 e^{-\Phi/kT}]}{m \cdot c \cdot T (1 - T_a/T)} \approx \frac{\sim T^2}{\sim T} \sim T \quad \rightarrow \quad \boxed{\frac{I_E}{P_{el}} \sim T} \quad (2).$$

It means in effect: The emission efficiency is increasing with higher cathode temperature T (for higher I_E). In this regime TE has a **positive trend**.

→ FE: The field emission FE has a **negative trend** (cf. FN plot): $\nu_{3E_FE} = \boxed{\frac{I_E}{P_{el}} = \frac{1}{U_{extr}}} \quad (3).$

The emission efficiency is decreasing with higher extraction voltage U_{extr} and so for higher emission

current I_E , cf. FN equation: $J_E = \frac{I_E}{A_C} = A \frac{E_{loc}^2}{\Phi} e^{-B \cdot \Phi^{1.5} / E_{loc}} \quad (4),$ with $E_{loc} = \gamma \cdot E_{extr} = \gamma \frac{U_{extr}}{d} \quad (5).$

Comparison of field (FE) and thermal (TE) cathodes

Vacuum tube DC 70 (triode) with directly heated hot filament cathode

SUBMINIATURE U.H.F. TRIODE DC 70

The DC 70 is a directly heated triode intended for purposes of transmitting and receiving at ultra high frequencies. It can for instance be used as an oscillator, amplifier, super-regenerative detector or mixer in walkie-talky equipment, balloon sondes, Citizens Radio or professional equipment, etc. When the tube is used as an oscillator, the output obtainable at 500 Mc/s ($\lambda = 60$ cm) is about 450 mW.

The filament voltage of the DC 70 is 1.25 V at a current of 0.2 A. Being a directly heated tube, its mutual conductance is high (3.4 mA/V at an anode current of 12 mA); the amplification factor amounts to 14.

The DC 70 is provided with leads which pass through the base and are to be soldered directly to the wiring of the circuit. For this reason no tube socket is used.

The small dimensions and battery operation make the DC 70 specially suitable for use in portable equipment. The tube can be mounted in all positions.

TECHNICAL DATA

FILAMENT DATA

Heating: direct by battery

Filament voltage $V_f = 1.25$ V

Filament current $I_f = 0.20$ A

$P_f = 0,25$ W

OPERATING CHARACTERISTICS AS AN OSCILLATOR AT

Anode voltage $V_a = 150$ V

Cathode current $I_k = 20$ mA

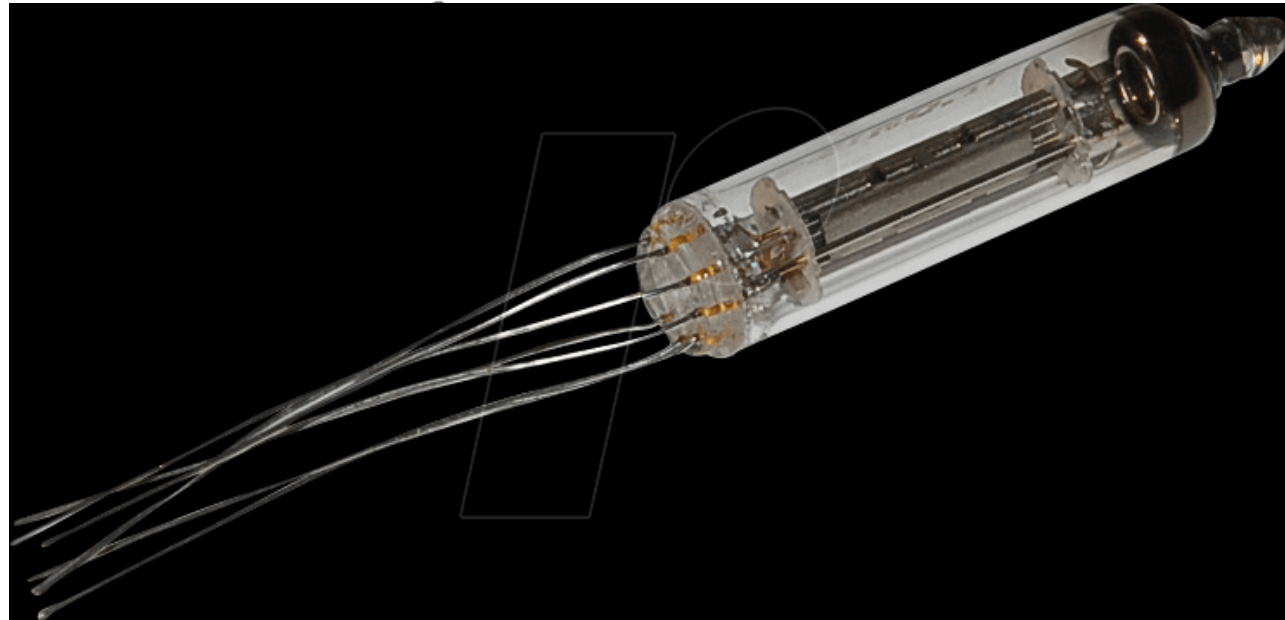


Fig. 1. Photograph of the DC 70 (actual size).

$P_f = 0,25$ W and $I_k = 20$ mA

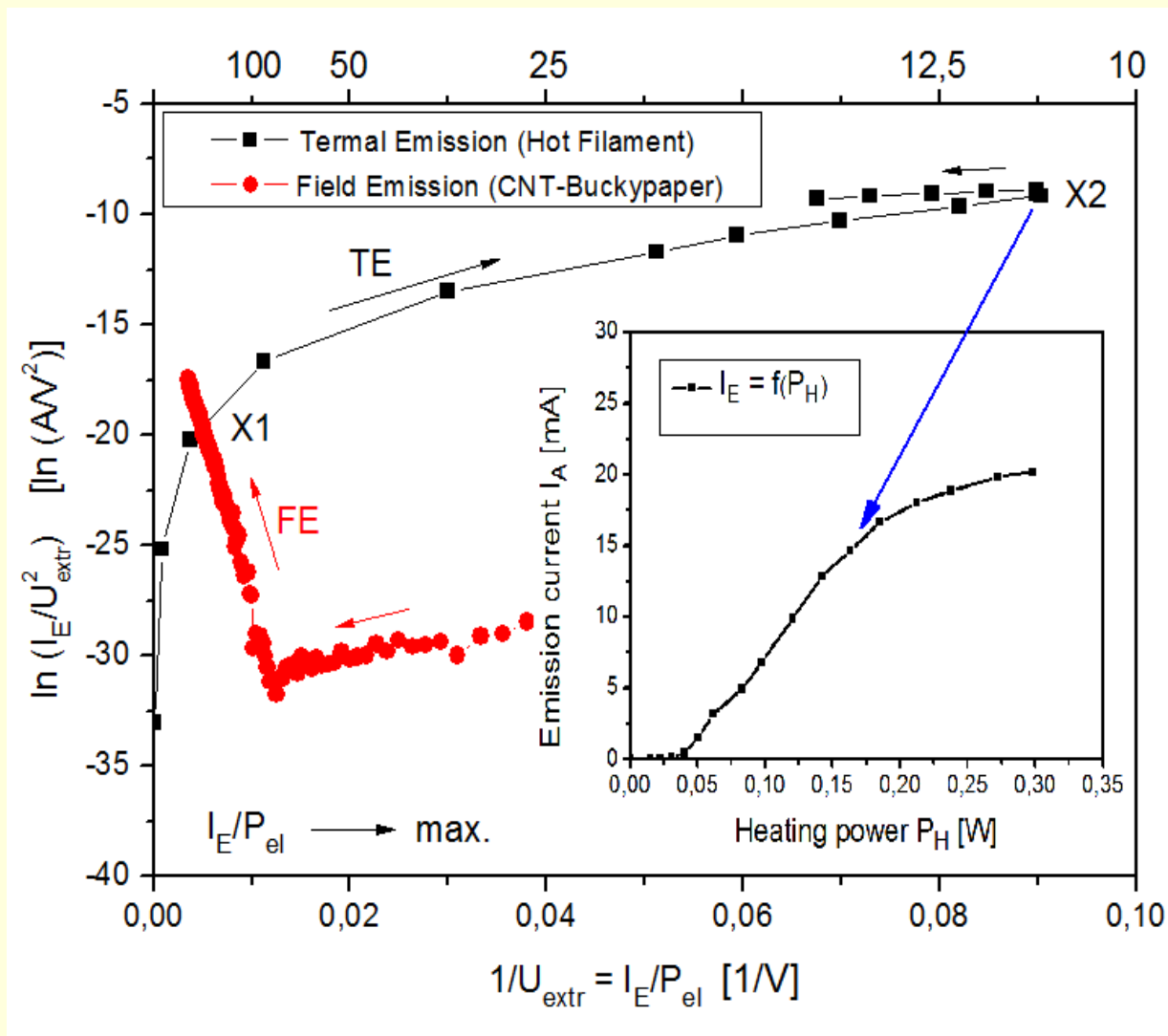
Emission efficiency: **$I_k/P_f = 0,08$**

Fictive voltage: **$U_{extr}^* = 12,5$ V**

Actual price: **5,35 € (Germany)**

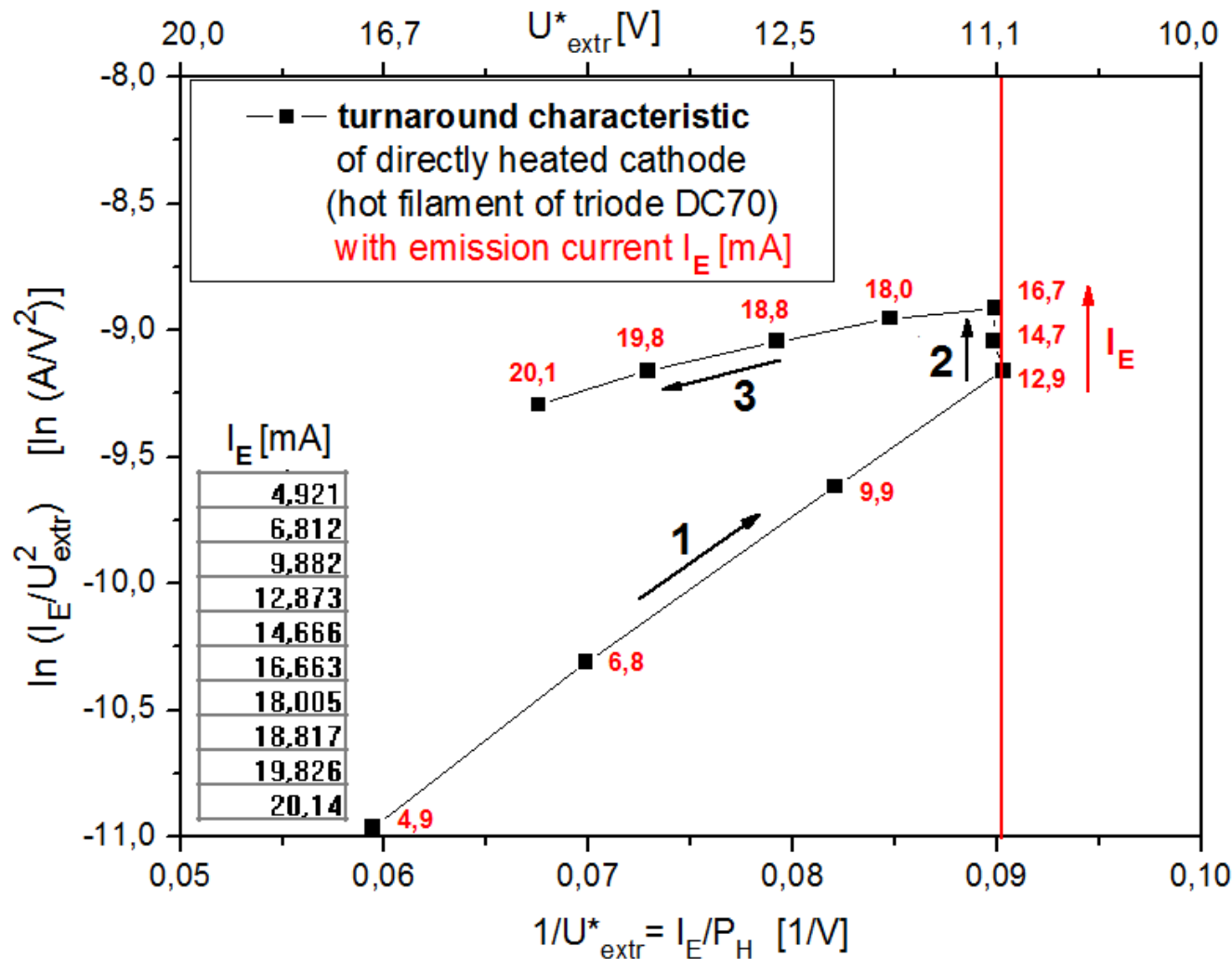
Lit.: Data sheet DC70: https://cdn-reichelt.de/documents/datenblatt/A300/DC70_DB-EN.pdf

Comparison of field (FE) and thermal (TE) cathodes



FN plot comparison of field (CNT-FE) and thermal cathodes (hot filament of DC70)

Comparison of field (FE) and thermal (TE) cathodes

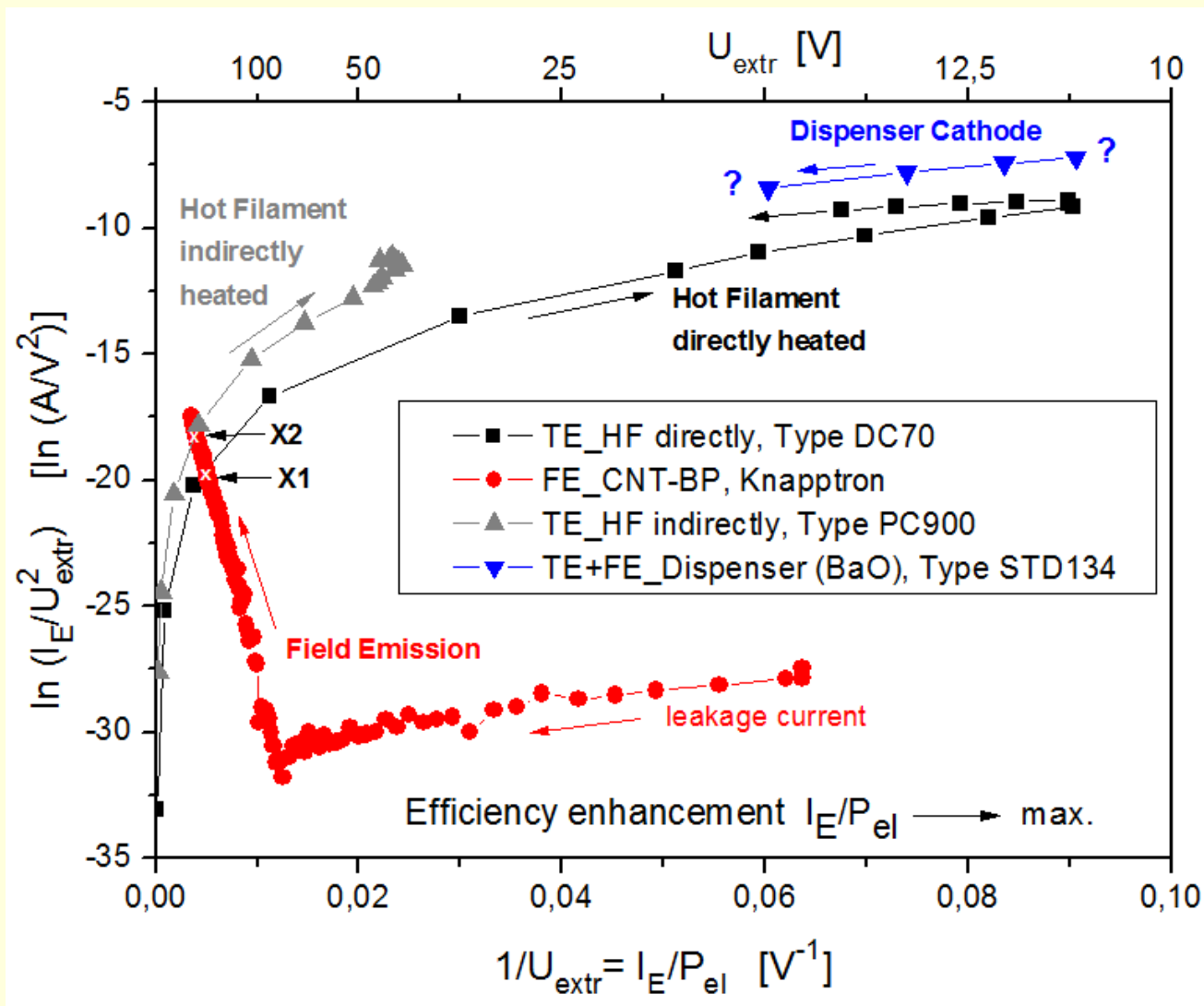


TE emission efficiency in the three curve sections:

- 1 $\frac{I_E}{P_{el}} \sim T$
Increasing with $T \uparrow$
- 2 $\frac{I_E}{P_{el}} = \text{const.}$
- 3 $\frac{I_E}{P_{el}} = \frac{I_E}{P_{heat} + P_{loss}}$
Decreasing with $P_{loss} \uparrow$

FN plot analysis of TE (hot filament) with three significant curve sections and corresponding trends of electron emission efficiencies at higher temperature T (right).

Comparison of field (FE) and thermal (TE) cathodes



FN plot comparison of all investigated FE and TE cathodes

Extended use of Fowler Nordheim plot Energetic evaluation of charge transfers

For novel investigations of the transition from field emission to stable plasma discharges an extended use of FN plot is proposed.

For this the inverse voltage (x-axis of the FN plot) is extended with factor 1 (= $I \cdot t / U \cdot I \cdot t$):

$$1/U = I \cdot t / U \cdot I \cdot t = Q/E \quad (1),$$

where U is the voltage, I the current, t the time, Q the sum of all transported charges and E the energy required for this.

The ordinate of Fowler-Nordheim plot will be unchanged.

The relation Q/E is a possible option for energetic evaluation.

The **operation compass** is important for basic orientation.

The direction Q/E maximum (red arrow or x-axis: $1/U$) is the direction of energetically optimal charge transfer.

It can be seen in Fig. 1 and Fig. 2 (next slide) that the micro-arc discharge has the highest charge transfer with the least energy input.

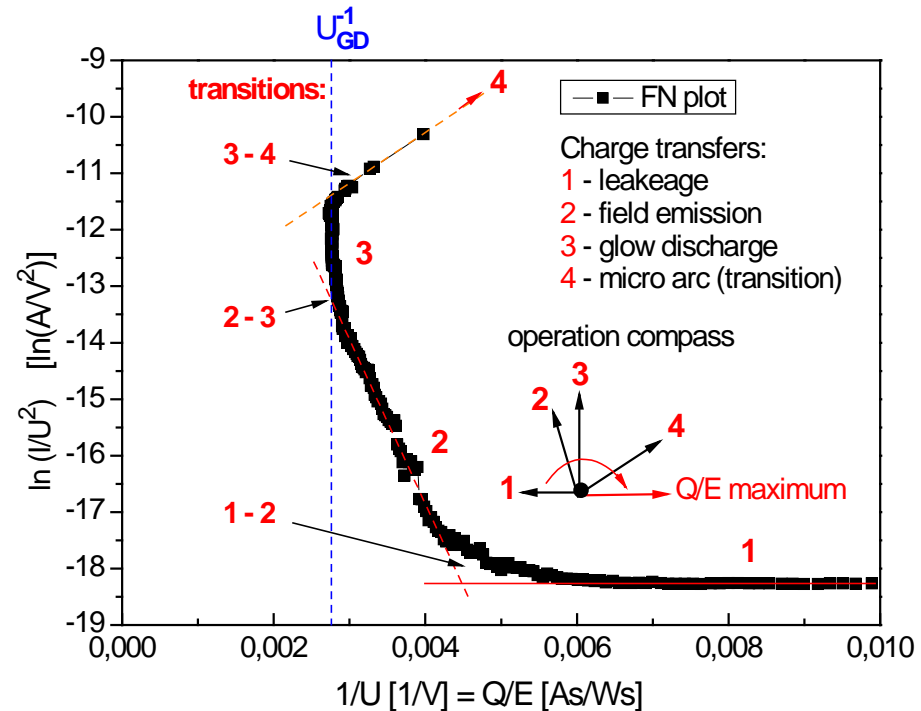


Fig. 1. FN plot of presented measurement SS3 [1] with smooth transitions. U_{GD} is the constant voltage of normal glow discharge.

[1] W. Knapp "Field-emission investigations of micro-structured stainless steel 1.4301 (ASTM 304) for extended use of vacuum components as very large FE cathode rrays." Poster, IVNC 2017.

Extended use of Fowler Nordheim plot Energetic evaluation of charge transfers

$R_s = 100 \text{ k}\Omega$, FE-cathode: stainless steel SS3 [1]

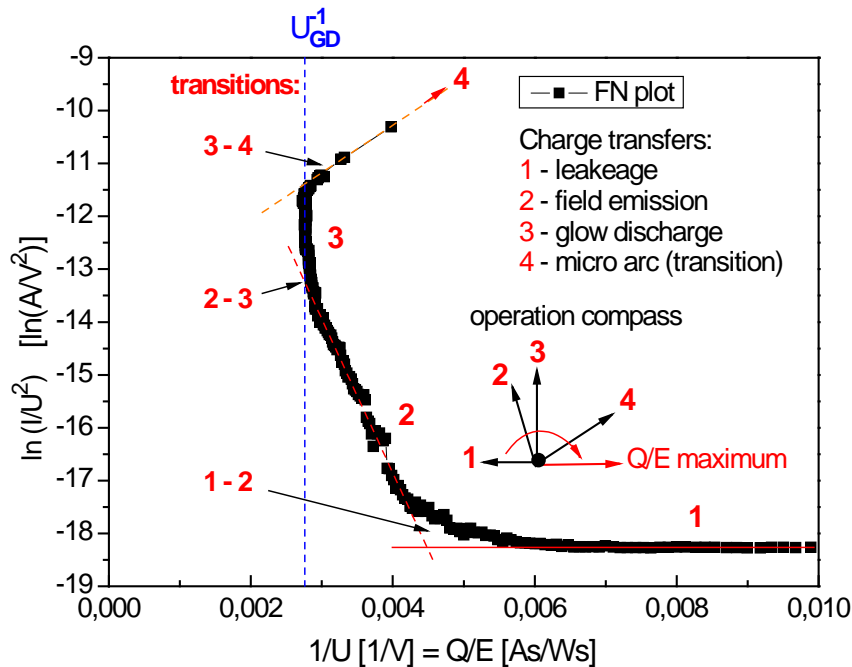


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[1] W. Knapp "Field-emission investigations of micro-structured stainless steel 1.4301 (ASTM 304) for extended use of vacuum components as very large FE cathode arrays." Poster, IVNC 2017.

[2] W. Knapp, C. Langer, C. Prommesberger, M. Lindner, R. Schreiner, "Investigations of the transition from field electron emission to stable plasma discharge in a micro electron source at vacuum pressure." Poster contribution, IVNC 2017.

$R_s = 10 \text{ M}\Omega$, FE-cathode: array of Si-tips [2]

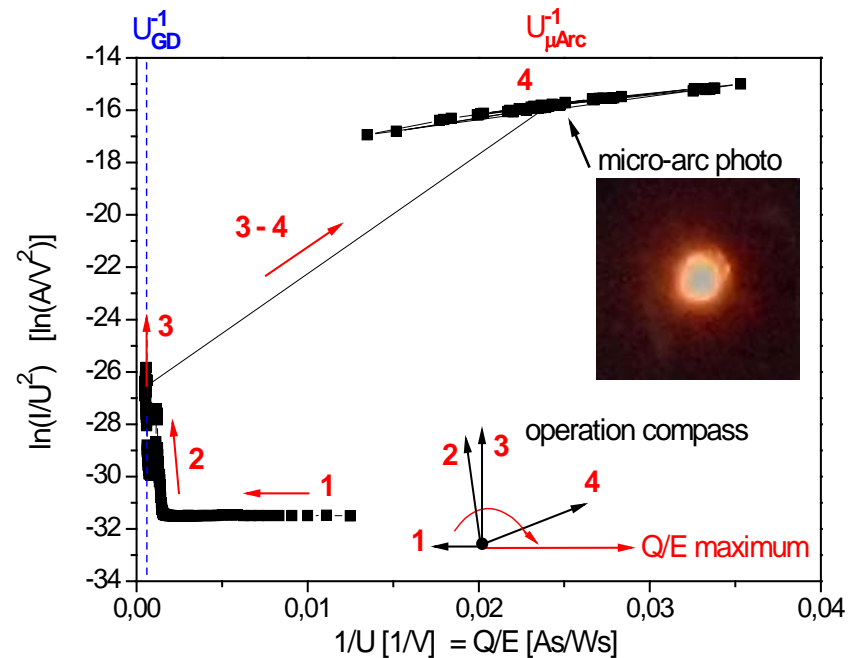


Fig. 2. FN plot for energetic evaluation of the transition from field electron emission to plasma discharges, as presented and detailed explained in [2, 3], with: **1** – leakage current, **2** – field emission, **3** – normal glow discharge, **3 - 4** – glow-to-arc transition, **4** – micro-arc discharge.

[3] D. Wenger, W. Knapp, B. Hensel, S. T. Tedde, "Transition of Electron Field Emission to Normal Glow Discharge", IEEE Transaction on Electron Devices 61 (11), p. 3864 (2014).

Conclusion and outlook

1. An extended use of FN plot is proposed for comparison of electron emission efficiency, in particular for field (FE) and thermal (TE) cathodes.
2. For this the inverse extraction voltage of field emission (x-axis of FN plot) is extended with factor I_E/I_E : $\frac{1}{U_{extr}} = \frac{I_E}{P_{el}}$.
3. The relation I_E/P_{el} , easy to measure (e.g. for TE is $P_{el} = P_{heat}$), is therefore a simple criterion reflecting the electron emission efficiency, independent of the kind of electron emission mechanism.
4. The comparison of different electron emission mechanism is based on the calculation of a fictive extraction voltage, e.g. for thermal emission: $U_{extr}^* = P_{heat}/I_E$.
5. First comparison results of emission efficiency of FE and TE cathodes are:
 - For higher current I_E : TE has an increasing and FE has a decreasing emission efficiency!
 - The cross-over point X of characteristics has a current value e.g. of $I_{E_X} = 117 \mu A$.
 - For $I_E > I_{E_X}$ TE (hot filament cathode of vacuum tube DC70) becomes more efficient.
 - For currents $I_E < I_{E_X}$ FE cathodes (investigated with CNT emitter) are more efficient.
 - FE requires more voltage U_{extr} for higher emission current I_E . With higher voltage a transition to plasma discharge are more likely to take action, if $I_E > 1.0 mA$.
6. The influence of power loss on the emission efficiency must be investigated more!

Thank you very much for your attention!



The author Wolfram Knapp as Otto von Guericke, IVNC 2017, Walhalla Regensburg / Donaustauf, Bavaria

Knapp, Wolfram: „Using Fowler-Nordheim plot for the comparison of electron emission efficiency of field (FE) and thermal emission (TE) cathodes. 7th ITG International Vacuum Electronics Workshop (IVEW) 2020 and 13th International Vacuum Electron Sources Conference (IVeSC) 2020 , planned for Physikzentrum Bad Honnef (PBH), Germany (virtual conference/Thales AVS France), May 26-29, 2020, Lecture IVEW23, May 26, 2020, 3:30 pm MESZ.